



10242 Glendon Drive Subdivision

Servicing & Stormwater Management Report

Project Location:

10242 Glendon Drive, Komoka, ON

Prepared for:

Sifton Properties Limited
London , ON

Prepared by:

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MTE File No.: 55926-100



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- Appendix 1 Location Plan
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1.0 INTRODUCTION

MTE Consultants Inc. (MTE) was retained by Sifton Properties Limited to complete a Servicing Report for 10242 Glendon Drive. The development is a residential subdivision development approximately 17.81Ha in size.

The site is located at the north-west of the Glendon Drive and Crestview Drive in the Komoka Ontario. The property is bounded to the north by CN Railway property, to the west by existing agricultural and commercial land, and to the east by agricultural and institutional lands.

This report details the municipal service (water, sanitary, storm) for the proposed development. A Location Plan for the proposed site is included in **Appendix 1**.

Background Documents

The following background materials were reviewed and referenced for the subject development:

- Middlesex Centre Settlement Area Stormwater Master Plan (Stantec, 2020)
- Preliminary Geotechnical Investigation (EXP, 2023)
- Preliminary Stormwater Management Strategy (Dillon, 2024)
- Phase 1 Environmental Assessment (EXP, 2023)

2.0 WATER

2.1 General

Water is available from the existing 300mm watermain on Glendon Road. Given the size of the project and proposed number of units, a looped service will be required. It is noted that the concept provided shows only one road connection to Glendon Road. If this should be the case, a secondary feed through one of the private blocks fronting onto Glendon Road will be required until such time as development of one of the neighbouring properties provides a secondary connection.

2.2 Criteria

The water distribution design criteria for the subject site, as provided by Municipality of Middlesex Centre are as follows:

- Operating pressures during all domestic scenarios shall be between 275-550 kPa;
- Operating pressures shall not fall below 140 kPa during the Max Day + Fire Flow Scenario; and
- Demands and material properties shall be designed in accordance with the Municipality of Middlesex Centre Design Criteria

2.2.1 Existing Conditions and Infrastructure

- Proposed grades within the subdivision vary between 247.81 and 251.69 masl.;
- The proposed subdivision will connect to:
 - Existing 300mm watermain on Glendon Drive

- A 300mm stub will be installed on Glendon Drive at Street “A” and a 300mm stub will be installed in front of Block 21 to be looped through Block 21 and Block 19 connecting to a 300mm watermain on Street ‘B’.
- A hydrant test was provided by the Municipality located at Tunks Lane near the Glendon Road Intersection.

2.2.2 Capacity

As detailed in this report, the existing water distribution infrastructure can supply the required domestic and fire suppression flows at pressures which meet or exceed the Municipality’s minimum requirements

2.2.3 External Works

No external water works are required for this development.

2.2.4 Effect of Development on Existing Infrastructure

No negative effects or conflicts with the existing infrastructure are anticipated as a result of the proposed development. Future development to the east and west will provide an additional loop between the proposed stubs.

2.2.5 Oversizing

No oversizing of infrastructure is required for this project.

2.2.6 Water system Area Plans

A ‘Watermain Layout Figure’, **Figure 2.1**, is attached in **Appendix 2**.

2.2.7 Water Network Analysis

Modelling of the proposed subdivision has been completed and is further described in the following sections.

2.2.8 Water Services

Proposed water services for the residential lots will be 25mm PEX as per Municipal standards.

2.3 Water Distribution Modelling

The water distribution modelling for the site was completed using WaterCAD. The site was modelled using a series of nodes connected by pipes. Demands were applied at the nodes and attributes assigned to the connecting pipes in keeping with City standards.

Future connections to the lands east and west of the development have been provided for. Demands for the future residential areas north of the site were considered conceptually. Future development to the east will provide a loop between the proposed stubs on Street ‘B’ and Glendon Drive and the future development to the west will provide a loop between the stub on Street ‘B’ and Tunks Lane.

Water supply was modelled as one reservoir situated at the connection point to the existing system. A rough sketch of the model network is included along with detailed calculations and modelling result summaries. Modelling assumptions and rationale are detailed further in the following sections.

2.3.1 Water Supply

Water supply for the proposed subdivision was modelled as 1 reservoir based on a hydrant flow test which was obtained from the Municipality. The test was completed at an existing hydrant on Tunks Lane near the Glendon Road Intersection. Refer to **Appendix 2** for the hydrant flow test report.

- Based on the hydrant test and adjusting for elevation changes the following data was inputted into model (see **Appendix B**):

Scenario	Flow (L/s)	Head (m)
Shutoff	0.00	33.17
Residual	90.72	21.85
Max Operation (20 psi)	139.56	8.07

2.3.2 Demands

The proposed internal network was modelled as a series of nodes and pipes. The nodes were placed at strategic locations within the proposed site and future development. Demands were assigned to the nodes based on their proximity to the surrounding lots. Demands were assigned to nodes based on the number of units in the vicinity, a population of 3 & 2.4 persons per low density and medium density units respectively, and an average day consumption of 350 L per person. Peaking factors of 2.0 and 3.0 were used for the max day and peak hour scenarios respectively in keeping with Municipal standards. Detailed demand calculations are included in **Appendix 2**.

2.4 Results

2.4.1 Domestic and Fire Flows (Including Future Developments)

AVERAGE DAY

Under this scenario, the minimum pressure in the system was computed to be 309 kPa (>275 kPa minimum required). Future demands were included, full summary modelling results are included in **Appendix 2**.

PEAK HOUR

Under this scenario, the minimum pressure in the Phase 3 system was computed to be 275 kPa (>275 kPa minimum required). Future demands were included. Full summary modelling results are included in **Appendix 2**.

MAX DAY + FIRE

For maximum day + fire 12 scenarios were completed applying a fire flow of 76.00L/s at each of the 9 proposed hydrant locations and 80 L/s at the medium density nodes (J-21, J-22 & J-23), as shown on 'Fire Flow Results' table below. A fire flow analysis was completed to determine the maximum fire flow available using a maximum velocity constraint of 2.4 m/s and minimum pressure constraint of 140 kPa. The result of each scenario is outlined below. Full summary modelling results are included in **Appendix 2**.

Fire Flow Results

Node	Available Flow (L/s)	Min Flow (L/s)	Max. Velocity (m/s)	Max. Allowed Velocity (m/s)
HYD-1	80.09	76.0	1.62	2.40
HYD-2	79.71	76.0	1.61	2.40
HYD-3	79.47	76.0	1.61	2.40
HYD-4	79.71	76.0	1.99	2.40
HYD-5	79.95	76.0	1.62	2.40
HYD-6	79.48	76.0	1.61	2.40
HYD-7	78.19	76.0	1.59	2.40
HYD-8	77.73	76.0	1.59	2.40
HYD-9	76.67	76.0	1.57	2.40
J-21	81.21	80.0	1.62	2.40
J-22	82.16	80.0	1.62	2.40
J-23	85.11	80.0	1.62	2.40

2.5 Quality Turnover

Quality turnover was modelled as an age analysis with a maximum allowable age of 72 hrs. The max age in the system was determined for full buildout of the site and future adjacent sites to the east and west. At full buildout the maximum age within the system was modelled to be approximately 14.3 hrs at J-16.

3.0 SANITARY

3.1 General

The site was accounted for in the design of the sanitary sewer system on Crestview Drive. As per the sanitary drainage area plan prepared for the Kilworth Heights West Subdivision (ENG PLUS, 2018), refer to **Appendix 3**, the site was accounted for with a population of 3486, which is approximately 100 persons per hectare. Given the size of the site a total population of 1781 persons would have been allocated for the site.

Sanitary servicing is proposed to be provided by connection to the existing 300mm sanitary sewer on Crestview Drive at Glendon Drive. (Refer to **Figure 3.1** in **Appendix 3**)

3.2 Proposed Design Flow

Based on the proposed sites land use the peak flows in the design of the local sewers was 32.69L/s. (Refer to the table and calculations on below)

Land Use	Area (Ha.)	Unit per Ha.	Units	People per Unit	Total Population
Single Family	3.90	30	117	3.0	351
Street Townhomes	1.45	75	109	2.4	262
Cluster Townhomes	3.94	75	296	2.4	711
Mixed Use	2.06	75	155	2.4	372
Totals					1696

Using the Municipal standard consumption rate of 350 L/person/day and a peaking factor of 4.5, a peak sanitary flow of:

$$1696 \text{ persons} \times 350 \text{ L/day} / 86,400 \text{ s/day} \times 4.5 = 30.91 \text{ L/s}$$

Infiltration is considered using the Municipal standard of 8640 L/ha/day:

$$17.81 \text{ ha} \times 8640 \text{ L/ha/day} / 86,400 \text{ s/day} = 1.78 \text{ L/s}$$

As the proposed population is less than the allocated population per Kilworth Heights Subdivision sanitary sewer design, no negative downstream impacts are anticipated.

4.0 STORMWATER

4.1 Criteria

The stormwater management design criteria for the subject site, as provided by the Municipality of Middlesex Centre and the Upper Thames River Conservation Authority (UTRCA) are as follows:

- Attenuation of the post-development peak flows for the 25mm through 100-year storm events to the pre-development (existing) peak flow rates;
- Implementation of water quality controls to provide Level 1 (enhanced) treatment levels as per the MOECC SWM Practices Planning and Design Manual (2003); and

4.2 Methodology

In order to successfully complete the stormwater management design for this site, the following specific tasks were undertaken:

- Determined the allowable/pre-development flow rates;
- Estimated the percent impervious of the site and catchment area parameters for inclusion in hydrologic modelling;
- Preliminary design of proposed SWM facility; and
- Modelling and design of controls to attain the required runoff rates.

4.3 Allowable/Pre-development Flow Rate

The site currently consists primarily of an undeveloped agricultural field which drains west to an adjacent woodlot and east to existing agricultural field. Runoff from the proposed site is to be captured and conveyed to the proposed SWM facility located at the north west end of the site. The proposed pond is intended to be a constructed dry SWM facility.

Pre-development conditions of the site were modelled using SWMHYMO modelling software to capture the existing drainage conditions of the site and the resulting flow rates to the wetland. Pre-development modelling information is further discussed in the sections below.

4.3.1 Topographical Information

A topographical survey of the site was completed by Trueline Service Inc. in April of 2025. Existing elevations across the site range from 251.80 in the northeast to 244.78 in the west. The site has undulating topography, with the overall fall towards the west property line and a smaller catchment area to the east.

4.3.2 Geotechnical Information

A geotechnical investigation of the site was completed by EXP. in September of 2023. The investigation consisted of the drilling of 11 boreholes within the site to depths ranging from 5.0m to 6.6m. The borehole data collected indicated the surficial topsoil depths ranged from 0.075m to 0.53m in depth (average ~0.41m). Sub-surface soils are generally comprised of sand and gravel with trace silt.

4.3.3 Hydro-geotechnical Information

As part of the geotechnical investigation, 4 monitoring wells were installed around the perimeter of the site and stabilized water elevations were recorded. The recorded elevations range from 242.94.0-246.25 and indicate a hydraulic gradient to the southeast.

4.3.4 Pre-Development Modelling

The following table summarizes the catchments used in the modelling of the site. The predevelopment condition was separated into 2 catchment areas representing the existing field (catchments 101-102). Catchment 101 represents the west side of the field which drains to the west limit of the woodlot, catchment 102 represents the east side of the field which drains to the adjacent agricultural property to the east. **Figure 4.1** illustrates the limits of the predevelopment catchment areas internal to the site.

Table 4-1 - Pre-Development Catchment Parameters

No.	Catchment	Area (ha)	% Impervious	Pervious CN	Impervious CN	Slope (%)	Flow Length (m)
101	TRIBUTARY WEST OF PROPERTY	14.66	0	75	98	0.93	525
102	TRIBUTARY EAST OF PROPERTY	3.16	0	75	98	0.77	210

Resulting Peak flow rates to the existing woodlot and adjacent lands to the east are summarized in the table below. These flow rates will serve as the target flow rates for the post development condition. Modelling output files are provided in **Appendix 4**.

Table 4-2 - Pre-Development Flow Rates

No.	25mm	2-year	5-year	10-year	25-year	50-year	100-year
Total to EP1 (Area 101)	0.076	0.156	0.293	0.404	0.553	0.672	0.798
To EP2 (Area 102)	0.021	0.044	0.084	0.117	0.160	0.195	0.232

4.4 Proposed SWM Strategy

4.4.1 General SWM Approach

The SWM strategy for the proposed development will be to capture a majority of the runoff from the proposed site and direct it toward the proposed dry SWM pond facility. Internal grading will be designed to direct minor system runoff to an internal storm sewer system while overland flow routes will be provided in the case of major system events. The proposed SWM facility will be designed to provide quality and quantity control for the entire site.

4.4.2 Quality Control

The proposed SWM facility has been designed as a dry pond with an active storage depth of 2.2m and a free board of 0.30m. As part of the ultimate solution, the pond could be designed as a dry pond facility with an infiltration component to achieve quality control and water balance for the site. The Infiltration could be used as the primary outlet for the facility, as explained in the 'Quantity Control' section.

An OGS will be incorporated into the storm system upstream of the dry pond to pre-treat events up to the 2-year storm sized to provide an enhanced level of control for the site. Since the majority of annual rainfall occurs in storms less than or equal to a 25mm event, the majority of water borne sediment is also transported to the stormwater management facilities in these less intense events. Furthermore, since larger storm events will have greater peak flows, there is potential for re-suspension of accumulated sediment within the OGS. To achieve this objective, it is proposed that the overland flows generated by major events be directed into the dry pond directly.

4.4.3 Quantity Control

Flows for all storm events will be conveyed to the stormwater management facility by a combination of storm sewer and overland flow route. Detailed design calculations and the post-development SWMHYMO design event modeling output are included in **Appendix 4**.

This facility contains an outlet control weir structure to control events up to the 250-year event and will be designed as part of the detailed engineering of the pond.

Infiltration through the bottom of the SWM facility will be used as the primary outlet for the facility, up to the 100-year storm event. It was noted in the geotechnical investigation that moderate to

significant rates of infiltration were to be expected during excavation below the groundwater table. Thus, it is assumed that the native soils have high hydraulic conductivity. For the purposes of this analysis a factored infiltration rate of 15mm/hr was assumed (minimum recommended for infiltration measures). Based on the conceptual pond area and infiltration rate, a flow rate of 26L/s can be achieved via infiltration.

The infiltration is represented as EP1 on **Figure 4.3** and EP2 represents any overflow to the adjacent woodlot in events that exceed 100-year event up to a 250-year event. The stage storage discharge relationship of the pond is summarized in **Table 4-3**.

The peak storage, and outflow for the conceptual facility during the various design storms are shown in **Table 4-4**. Design parameters for the facility are summarized in **Table 4-5** and the location of the proposed facility is provided in **Figure 4.2**.

Table 4-3 – Pond Stage Storage Discharge Summary

Stage (masl)	Peak Storage (m ³)	Discharge (infiltration) (L/s)
246.50	0.00	0.00
246.55	312.10	25.67
247.00	3154.05	25.67
247.50	7486.00	25.67
247.70	10103.9	25.67

As per the 'Preliminary Geotechnical Investigation' by EXP dated September 1, 2023, the high groundwater elevation in the general area of the proposed SWM facility is 243.08m, which is 3.42m below the bottom of pond. Based on this preliminary information, there should not be any ground water concerns.

Table 4-4 – Proposed Event Model Output

Storm Event	Peak Storage Requirement (m ³)	Peak Outflow (Infiltration) (L/s)
25 mm	2,068	26.0
2 Year	3,152	26.0
5 Year	4,720	26.0
10 Year	5,849	26.0
25 Year	7,248	26.0
50 Year	8,345	26.0
100 Year	9,440	26.0

Table 4-5 – SWM Facility Design Characteristics

General	Facility Characteristics
Stormwater Management Facility Type	Dry Pond
Required MOE Water Quality Protection	Enhanced
Total Contributing Area	17.33 ha
Imperviousness (Average)	44.6%
Bottom Elevation	246.50

4.4.4 Major and Minor Flow Routing

Based on the layout of the proposed subdivision, overland flow from the proposed road and Blocks will be required to flow through a proposed maintenance access block fronting the SWM block in order to reach the proposed SWM facility. Therefore, the grading and layout of proposed maintenance access block will need to be designed to provide a corridor which will accommodate major and minor flows from the upstream areas through the property.

Minor flows will be collected and conveyed west along the roads to the proposed SWM pond via storm sewers. Major flows from the road will be conveyed overland within the proposed ROW.

5.0 CONCLUSIONS

Based on the foregoing analysis, it is concluded that:

- i. the proposed development can be adequately serviced by the existing sanitary sewer on Glendon Drive
- ii. the proposed development will be serviced by the existing 300mm watermain feed from Glendon Drive. Additional looping will be provided for the area once the adjacent lands to the east and west are developed;
- iii. the proposed stormwater management design provides adequate attenuation of the 2 through 100-year storm events and provides adequate water quality control for the proposed site.

It is recommended that:

- iv. the site grading be designed to convey major system runoff to the SWM facility and minimizes cut/fill requirements for the site;
- v. the proposed servicing measures be fully designed and detailed as part of the detailed design process to the satisfaction of the Municipality of Middlesex Centre.

All of which is respectfully submitted,

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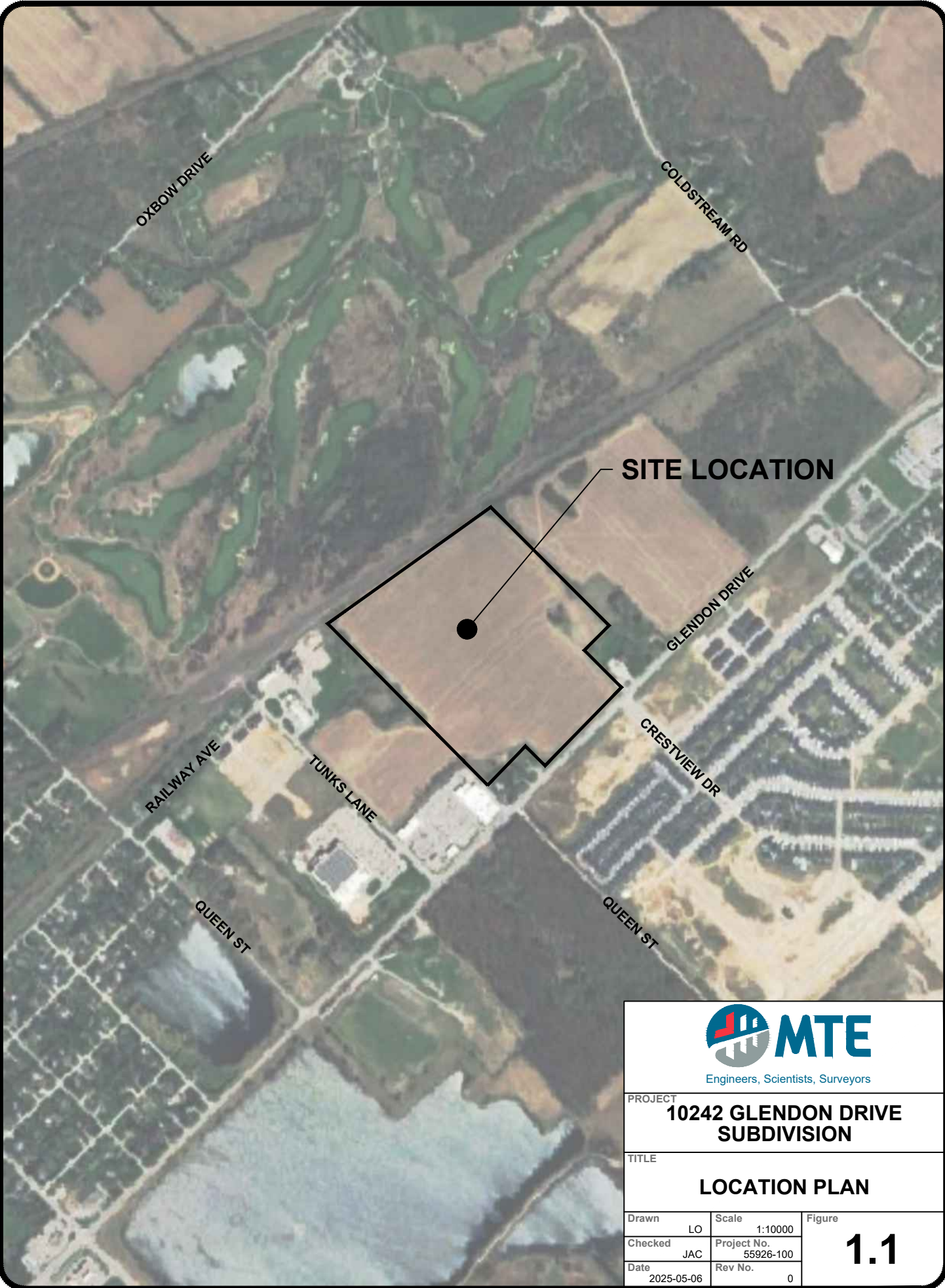
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Document1



Appendix 1

Location Plan





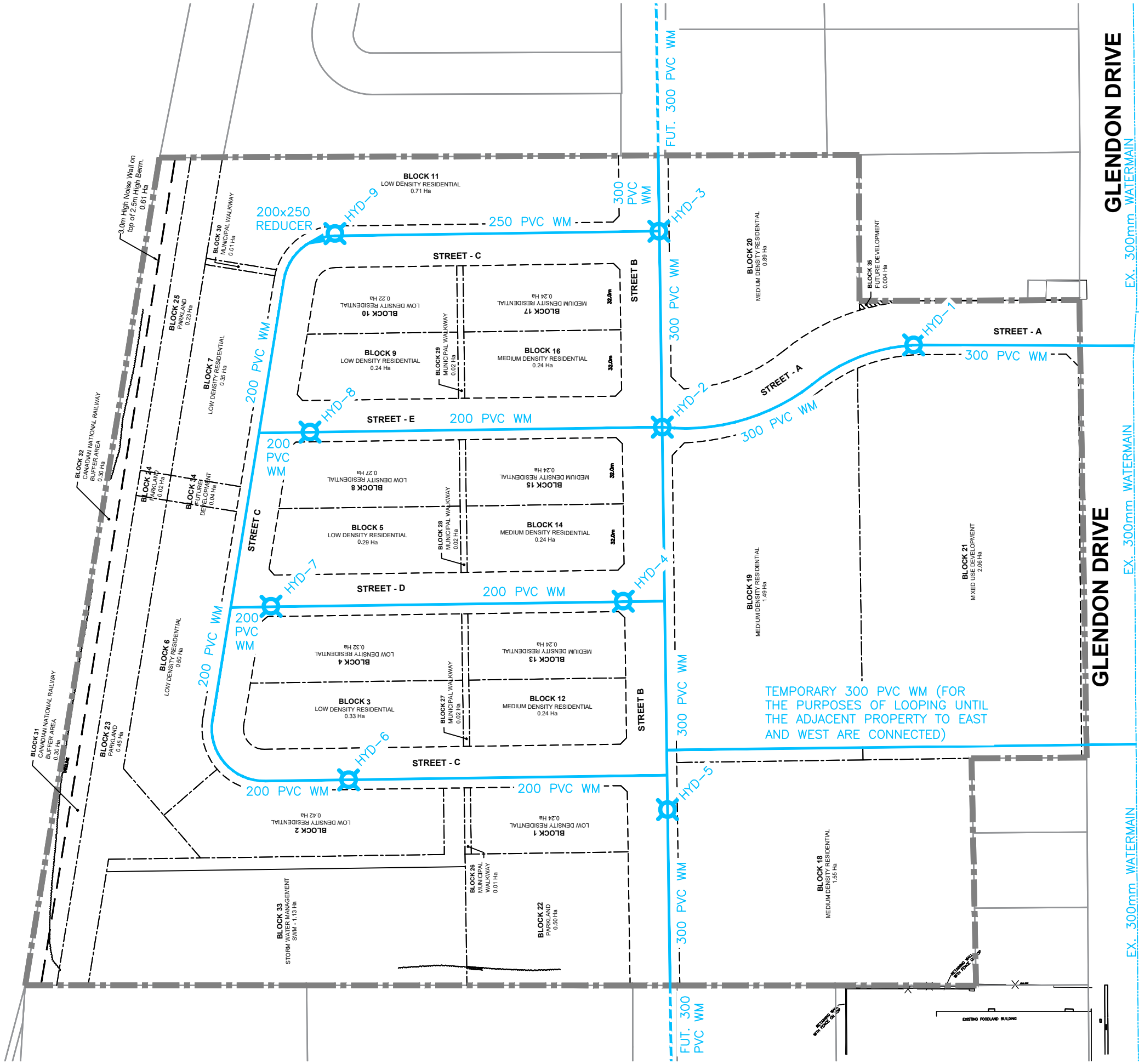
Engineers, Scientists, Surveyors

PROJECT		
10242 GLENDON DRIVE SUBDIVISION		
TITLE		
LOCATION PLAN		
Drawn	LO	Scale 1:10000
Checked	JAC	Project No. 55926-100
Date	2025-05-06	Rev No. 0

Figure 1.1

Appendix 3

Water Servicing Information



EX. 300mm WATERMAIN
CRESTVIEW DRIVE

GLENDON DRIVE
EX. 300mm WATERMAIN

GLENDON DRIVE
EX. 300mm WATERMAIN

EX. 300mm WATERMAIN



Engineers, Scientists, Surveyors

PROJECT
**10242 GLENDON DRIVE
SUBDIVISION**

TITLE
WATERMAIN LAYOUT

Drawn	LO	Scale	1:2000	Figure 2.1
Checked	JAC	Project No.	55926-100	
Date	2025-05-06	Rev No.	0	



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123 St. George St., London, Ontario N6A 3A1

DATE: May 27, 2025
JOB NO.: 55926-100

Project: 10242 Glendon Drive
Location: Komoka ON

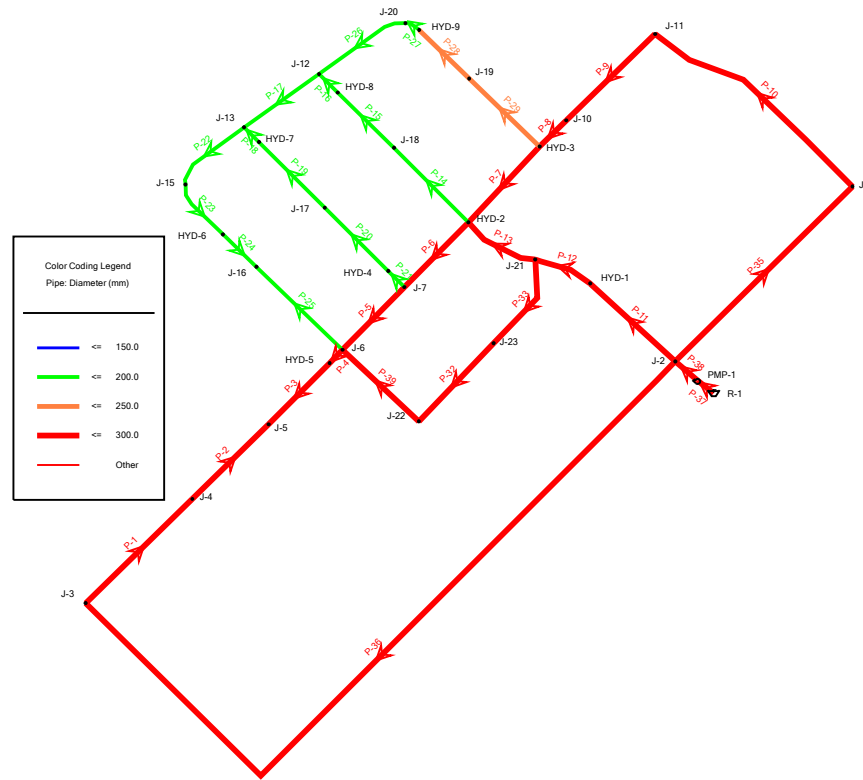
Water Demand Calculation

				Residential (Low Density)						Residential (Medium Density)						Demand Summary		
Building	Approximate Surface Elevation (mASL)	Approximate Elevation (mASL)	Node	Area (ha.)	Units/ha	PPL/Units	Pop	L/day/cap	Avg. Day Demand (l/s)	Area (ha.)	Units/ha	PPL/Units	Pop	L/day/cap	Avg. Day Demand (l/s)	Avg. Day (l/s)	Max Day (l/s)	Max Hour (l/s)
Adjacent Lands to the West	242.74	241.04	J-4	10.39	33.3	3.0	1038	350	4.21	0.00	75	2.4	0	350	0.00	4.21	8.42	12.63
Adjacent Lands to the East	247.90	246.2	J-11	-	-	-	1482	350	6.01	-	-	-	0	350	0.00	6.01	12.02	18.03
Street C	251.44	249.74	J-12	0.76	30	3.0	69	350	0.28	0.00	75	2.4	0	350	0.00	0.28	0.56	0.84
Street C	251.01	249.31	J-13	0.90	30	3.0	81	350	0.33	0.00	75	2.4	0	350	0.00	0.33	0.66	0.99
Street C	250.43	248.73	J-15	0.96	30	3.0	87	350	0.36	0.00	75	2.4	0	350	0.00	0.36	0.72	1.08
Street C	248.68	246.98	J-16	0.24	30	3.0	22	350	0.09	0.24	75	2.4	44	350	0.18	0.27	0.54	0.81
Street D	250.49	248.79	J-17	0.00	30	3.0	0	350	0.00	0.48	75	2.4	87	350	0.36	0.36	0.72	1.08
Street E	250.36	248.66	J-18	0.00	30	3.0	0	350	0.00	0.48	75	2.4	87	350	0.36	0.36	0.72	1.08
Street C	250.9	249.2	J-19	0.25	30	3.0	23	350	0.10	0.24	75	2.4	44	350	0.18	0.28	0.56	0.84
Street C	251.76	250.06	J-20	0.79	30	3.0	72	350	0.30	0.00	75	2.4	0	350	0.00	0.30	0.60	0.90
Street A	249.94	248.24	J-21	0.00	30	3.0	0	350	0.00	0.89	75	2.4	161	350	0.66	0.66	1.32	1.98
Medium Density Block 18	249.57	247.87	J-22	0.00	30	3.0	0	350	0.00	1.55	75	2.4	279	350	1.14	1.14	2.28	3.42
Medium Density Block 19 & 21	249.98	248.28	J-23	0.00	30	3.0	0	350	0.00	3.58	75	2.4	645	350	2.62	2.62	5.24	7.86
Total				14.29			2874		11.68	7.46			1347		5.50	17.18	34.36	51.54

Design Specifications and Requirments Manual

Max Day Factor = 2.00
Peak Hour Factor = 3.00

Scenario: Maximum Day + Fire Flow



Hydrant Test (Model Pump Data)

Elev. At HYD	241.84	Elev. At Main	247.83
--------------	--------	---------------	--------

Scenario	Flow (L/s)	Head (m)
Shutoff	0	33.17
Design	90.72	21.85
Max. Operation	139.56	8.07



FLOWMETRIX
INDU-TECH
PROCESS

Fire Flow Testing Report

Residual Hydrant #
NFPA Colour Code

Ko-38
BLUE

DATE May 16, 2022
TIME 3:15 PM
ADDRESS Tunks Lane @ Glendon
SETTLEMENT AREA Komoka

MAKE Canada Valve
MODEL Century

RESIDUAL HYDRANT INFO.

HYDRANT # Ko-38
N.F.P.A. COLOUR CODE BLUE

STATIC PRESSURE 55.7 psi
RESIDUAL PRESSURE 39.6 psi

PRESSURE DROP 16.1 psi
% PRESSURE DROP 28.9 % psi

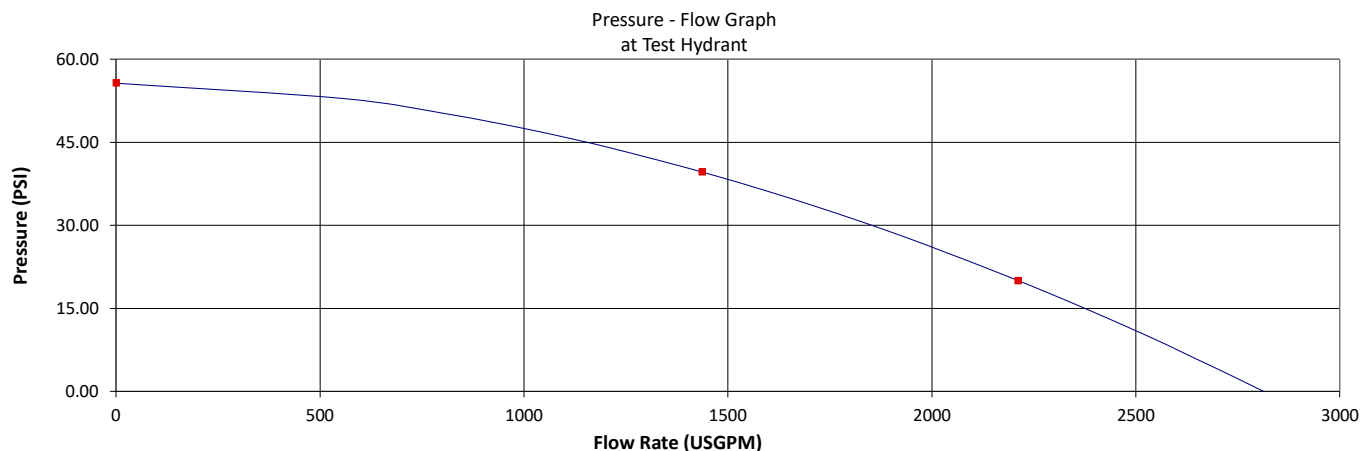
Flow on Water Main At Test Hydrant @ 20 psi 2212 USGPM



FLOW HYDRANT(S) INFO.

HYDRANT ASSET ID	HYD. # PORTS	OUTLET DIAMETER (INCHES)	NOZZLE COEFFICIENT	DIFFUSER TYPE	DIFFUSER COEFFICIENT	PITOT READING (psi)	PITOT FLOW (USGPM)	TOTAL VOLUME OF WATER (Gal)
Ko-109	2	2.5	Round	LPD250	0.90	22.7	1438	1140
		2.5	Round	LPD250	0.90	22.7	0	1140
		Total Flow						1438

FIRE FLOW CHART



COMMENTS

OPERATOR
OPERATOR
OPERATOR

FMX
FMX

Jordan Whitlock
Ryan Ritchie

10242 Glendon Drive Subdivision
Average Day Demand Scenario
Junction Table - Time: 0.00 hours

Label	Elevation (m)	Demand (L/s)	Hydraulic Grade (m)	Pressure (kPa)	Age (Maximum) (hours)	Block ID
HYD-1	247.87	0.00	281.47	329	(N/A)	
HYD-2	247.69	0.00	281.47	331	(N/A)	
HYD-3	248.02	0.00	281.47	327	(N/A)	
HYD-4	247.65	0.00	281.47	331	(N/A)	
HYD-5	246.84	0.00	281.46	339	(N/A)	
HYD-6	247.72	0.00	281.47	330	(N/A)	
HYD-7	249.22	0.00	281.47	316	(N/A)	
HYD-8	249.47	0.00	281.47	313	(N/A)	
HYD-9	249.90	0.00	281.47	309	(N/A)	
J-1	249.20	0.00	281.47	316	(N/A)	
J-2	247.18	0.00	281.47	336	(N/A)	
J-3	240.36	0.00	281.47	402	(N/A)	
J-4	241.04	4.21	281.47	396	(N/A)	
J-5	246.25	6.01	281.46	345	(N/A)	
J-6	246.96	0.00	281.47	338	(N/A)	
J-7	247.36	0.00	281.47	334	(N/A)	
J-10	248.20	0.00	281.47	326	(N/A)	
J-11	246.20	0.00	281.47	345	(N/A)	
J-12	249.74	0.28	281.47	311	(N/A)	
J-13	249.31	0.33	281.47	315	(N/A)	
J-15	248.73	0.36	281.47	320	(N/A)	
J-16	246.98	0.27	281.47	337	(N/A)	
J-17	248.79	0.36	281.47	320	(N/A)	
J-18	248.66	0.36	281.47	321	(N/A)	
J-19	249.20	0.28	281.47	316	(N/A)	
J-20	250.06	0.30	281.47	307	(N/A)	
J-21	248.24	0.66	281.47	325	(N/A)	
J-22	247.87	1.14	281.47	329	(N/A)	
J-23	248.28	2.62	281.47	325	(N/A)	

10242 Glendon Drive Subdivision
Average Day Demand Scenario
Pipe Table - Time: 0.00 hours

Label	Length (m)	Start Node	Stop Node	Diameter (mm)	Hazen-Williams C	Velocity (m/s)
P-1	139	J-3	J-4	300.0	120.0	0.11
P-2	99	J-4	J-5	300.0	120.0	0.05
P-3	80	J-5	HYD-5	300.0	110.0	0.04
P-4	17	HYD-5	J-6	300.0	110.0	0.04
P-5	82	J-6	J-7	300.0	120.0	0.04
P-6	85	J-7	HYD-2	300.0	120.0	0.04
P-7	97	HYD-2	HYD-3	300.0	120.0	0.03
P-8	35	HYD-3	J-10	300.0	120.0	0.05
P-9	115	J-10	J-11	300.0	120.0	0.05
P-10	235	J-11	J-1	300.0	120.0	0.05
P-11	107	J-2	HYD-1	300.0	120.0	0.09
P-12	56	HYD-1	J-21	300.0	120.0	0.09
P-13	73	J-21	HYD-2	300.0	120.0	0.02
P-14	98	HYD-2	J-18	200.0	110.0	0.02
P-15	73	J-18	HYD-8	200.0	110.0	0.01
P-16	25	HYD-8	J-12	200.0	110.0	0.01
P-17	86	J-12	J-13	200.0	110.0	0.02
P-18	19	J-13	HYD-7	200.0	110.0	0.00
P-19	86	HYD-7	J-17	200.0	110.0	0.00
P-20	83	J-17	HYD-4	200.0	110.0	0.02
P-21	21	HYD-4	J-7	200.0	110.0	0.02
P-22	79	J-13	J-15	200.0	110.0	0.02
P-23	60	J-15	HYD-6	200.0	110.0	0.01
P-24	43	HYD-6	J-16	200.0	110.0	0.01
P-25	111	J-16	J-6	200.0	110.0	0.00
P-26	95	J-12	J-20	200.0	110.0	0.02
P-27	15	J-20	HYD-9	200.0	110.0	0.03
P-28	65	HYD-9	J-19	250.0	110.0	0.02
P-29	91	J-19	HYD-3	250.0	110.0	0.03
P-32	101	J-22	J-23	300.0	120.0	0.02
P-33	94	J-23	J-21	300.0	120.0	0.06
P-35	1	J-2	J-1	300.0	120.0	0.05
P-36	1	J-2	J-3	300.0	120.0	0.11
P-37	1	R-1	PMP-1	300.0	120.0	0.24
P-38	1	PMP-1	J-2	300.0	120.0	0.24

10242 Glendon Drive Subdivision
Max Day Demand + Fire Flow Scenario
Junction Table - Time: 0.00 hours

Label	Elevation (m)	Demand (L/s)	Hydraulic Grade (m)	Pressure (kPa)	Age (Maximum) (hours)	Block ID
HYD-1	247.87	0.00	280.10	315	(N/A)	
HYD-2	247.69	0.00	280.09	317	(N/A)	
HYD-3	248.02	0.00	280.09	314	(N/A)	
HYD-4	247.65	0.00	280.08	317	(N/A)	
HYD-5	246.84	0.00	280.08	325	(N/A)	
HYD-6	247.72	0.00	280.08	317	(N/A)	
HYD-7	249.22	0.00	280.08	302	(N/A)	
HYD-8	249.47	0.00	280.09	300	(N/A)	
HYD-9	249.90	0.00	280.09	295	(N/A)	
J-1	249.20	0.00	280.11	303	(N/A)	
J-2	247.18	0.00	280.11	322	(N/A)	
J-3	240.36	0.00	280.11	389	(N/A)	
J-4	241.04	8.42	280.08	382	(N/A)	
J-5	246.25	12.02	280.08	331	(N/A)	
J-6	246.96	0.00	280.08	324	(N/A)	
J-7	247.36	0.00	280.08	320	(N/A)	
J-10	248.20	0.00	280.09	312	(N/A)	
J-11	246.20	0.00	280.10	332	(N/A)	
J-12	249.74	0.56	280.09	297	(N/A)	
J-13	249.31	0.66	280.08	301	(N/A)	
J-15	248.73	0.72	280.08	307	(N/A)	
J-16	246.98	0.54	280.08	324	(N/A)	
J-17	248.79	0.72	280.08	306	(N/A)	
J-18	248.66	0.72	280.09	308	(N/A)	
J-19	249.20	0.56	280.09	302	(N/A)	
J-20	250.06	0.60	280.09	294	(N/A)	
J-21	248.24	1.32	280.09	312	(N/A)	
J-22	247.87	2.28	280.08	315	(N/A)	
J-23	248.28	5.24	280.08	311	(N/A)	

10242 Glendon Drive Subdivision
Max Day Demand + Fire Flow Scenario
Pipe Table - Time: 0.00 hours

Label	Length (m)	Start Node	Stop Node	Diameter (mm)	Hazen-Williams C	Velocity (m/s)
P-1	139	J-3	J-4	300.0	120.0	0.21
P-2	99	J-4	J-5	300.0	120.0	0.09
P-3	80	J-5	HYD-5	300.0	110.0	0.08
P-4	17	HYD-5	J-6	300.0	110.0	0.08
P-5	82	J-6	J-7	300.0	120.0	0.08
P-6	85	J-7	HYD-2	300.0	120.0	0.09
P-7	97	HYD-2	HYD-3	300.0	120.0	0.07
P-8	35	HYD-3	J-10	300.0	120.0	0.10
P-9	115	J-10	J-11	300.0	120.0	0.10
P-10	235	J-11	J-1	300.0	120.0	0.10
P-11	107	J-2	HYD-1	300.0	120.0	0.17
P-12	56	HYD-1	J-21	300.0	120.0	0.17
P-13	73	J-21	HYD-2	300.0	120.0	0.04
P-14	98	HYD-2	J-18	200.0	110.0	0.05
P-15	73	J-18	HYD-8	200.0	110.0	0.02
P-16	25	HYD-8	J-12	200.0	110.0	0.02
P-17	86	J-12	J-13	200.0	110.0	0.05
P-18	19	J-13	HYD-7	200.0	110.0	0.01
P-19	86	HYD-7	J-17	200.0	110.0	0.01
P-20	83	J-17	HYD-4	200.0	110.0	0.03
P-21	21	HYD-4	J-7	200.0	110.0	0.03
P-22	79	J-13	J-15	200.0	110.0	0.03
P-23	60	J-15	HYD-6	200.0	110.0	0.01
P-24	43	HYD-6	J-16	200.0	110.0	0.01
P-25	111	J-16	J-6	200.0	110.0	0.01
P-26	95	J-12	J-20	200.0	110.0	0.04
P-27	15	J-20	HYD-9	200.0	110.0	0.06
P-28	65	HYD-9	J-19	250.0	110.0	0.04
P-29	91	J-19	HYD-3	250.0	110.0	0.05
P-32	101	J-22	J-23	300.0	120.0	0.04
P-33	94	J-23	J-21	300.0	120.0	0.11
P-35	1	J-2	J-1	300.0	120.0	0.10
P-36	1	J-2	J-3	300.0	120.0	0.21
P-37	1	R-1	PMP-1	300.0	120.0	0.49
P-38	1	PMP-1	J-2	300.0	120.0	0.49

10242 Glendon Drive Subdivision
Max Day Demand + Fire Flow Scenario
Fire Flow Results Table - Time: 0.00 hours

Label	Fire Flow (Needed) (L/s)	Flow (Total Available) (L/s)	Pressure (Calculated Residual) (kPa)	Junction w/ Minimum Pressure (System)	Pressure (Calculated Zone Lower Limit) (kPa)	Pipe w/ Maximum Velocity	Velocity of Maximum Pipe (m/s)
HYD-1	76.00	80.09	161	J-20	140	P-38	1.62
HYD-2	76.00	79.71	163	J-20	140	P-38	1.61
HYD-3	73.00	79.47	160	J-20	140	P-38	1.61
HYD-4	76.00	79.71	157	J-20	140	P-21	1.99
HYD-5	76.00	79.95	170	J-20	140	P-38	1.62
HYD-6	76.00	79.48	144	J-20	140	P-38	1.61
HYD-7	76.00	78.19	140	J-13	142	P-38	1.59
HYD-8	76.00	77.73	140	J-12	141	P-38	1.59
HYD-9	76.00	76.67	141	J-20	140	P-38	1.57
J-21	80.00	81.21	157	J-20	140	P-38	1.62
J-22	80.00	82.16	159	J-20	140	P-38	1.62
J-23	80.00	85.11	155	J-20	140	P-38	1.62

10242 Glendon Drive Subdivision
Peak Hour Demand Scenario
Junction Table - Time: 0.00 hours

Label	Elevation (m)	Demand (L/s)	Hydraulic Grade (m)	Pressure (kPa)	Age (Maximum) (hours)	Block ID
HYD-1	247.87	0.00	277.98	295	(N/A)	
HYD-2	247.69	0.00	277.96	296	(N/A)	
HYD-3	248.02	0.00	277.96	293	(N/A)	
HYD-4	247.65	0.00	277.95	297	(N/A)	
HYD-5	246.84	0.00	277.94	304	(N/A)	
HYD-6	247.72	0.00	277.95	296	(N/A)	
HYD-7	249.22	0.00	277.95	281	(N/A)	
HYD-8	249.47	0.00	277.95	279	(N/A)	
HYD-9	249.90	0.00	277.96	275	(N/A)	
J-1	249.20	0.00	278.01	282	(N/A)	
J-2	247.18	0.00	278.01	302	(N/A)	
J-3	240.36	0.00	278.01	369	(N/A)	
J-4	241.04	12.63	277.95	361	(N/A)	
J-5	246.25	18.03	277.94	310	(N/A)	
J-6	246.96	0.00	277.95	303	(N/A)	
J-7	247.36	0.00	277.95	299	(N/A)	
J-10	248.20	0.00	277.97	291	(N/A)	
J-11	246.20	0.00	277.98	311	(N/A)	
J-12	249.74	0.84	277.95	276	(N/A)	
J-13	249.31	0.99	277.95	280	(N/A)	
J-15	248.73	1.08	277.95	286	(N/A)	
J-16	246.98	0.81	277.95	303	(N/A)	
J-17	248.79	1.08	277.95	285	(N/A)	
J-18	248.66	1.08	277.95	287	(N/A)	
J-19	249.20	0.84	277.96	282	(N/A)	
J-20	250.06	0.90	277.96	275	(N/A)	
J-21	248.24	1.98	277.96	291	(N/A)	
J-22	247.87	3.42	277.95	294	(N/A)	
J-23	248.28	7.86	277.95	290	(N/A)	

10242 Glendon Drive Subdivision
Peak Hour Demand Scenario
Pipe Table - Time: 0.00 hours

Label	Length (m)	Start Node	Stop Node	Diameter (mm)	Hazen-Williams C	Velocity (m/s)
P-1	139	J-3	J-4	300.0	120.0	0.32
P-2	99	J-4	J-5	300.0	120.0	0.14
P-3	80	J-5	HYD-5	300.0	110.0	0.12
P-4	17	HYD-5	J-6	300.0	110.0	0.12
P-5	82	J-6	J-7	300.0	120.0	0.11
P-6	85	J-7	HYD-2	300.0	120.0	0.13
P-7	97	HYD-2	HYD-3	300.0	120.0	0.10
P-8	35	HYD-3	J-10	300.0	120.0	0.15
P-9	115	J-10	J-11	300.0	120.0	0.15
P-10	235	J-11	J-1	300.0	120.0	0.15
P-11	107	J-2	HYD-1	300.0	120.0	0.26
P-12	56	HYD-1	J-21	300.0	120.0	0.26
P-13	73	J-21	HYD-2	300.0	120.0	0.06
P-14	98	HYD-2	J-18	200.0	110.0	0.07
P-15	73	J-18	HYD-8	200.0	110.0	0.03
P-16	25	HYD-8	J-12	200.0	110.0	0.03
P-17	86	J-12	J-13	200.0	110.0	0.07
P-18	19	J-13	HYD-7	200.0	110.0	0.01
P-19	86	HYD-7	J-17	200.0	110.0	0.01
P-20	83	J-17	HYD-4	200.0	110.0	0.05
P-21	21	HYD-4	J-7	200.0	110.0	0.05
P-22	79	J-13	J-15	200.0	110.0	0.05
P-23	60	J-15	HYD-6	200.0	110.0	0.02
P-24	43	HYD-6	J-16	200.0	110.0	0.02
P-25	111	J-16	J-6	200.0	110.0	0.01
P-26	95	J-12	J-20	200.0	110.0	0.06
P-27	15	J-20	HYD-9	200.0	110.0	0.09
P-28	65	HYD-9	J-19	250.0	110.0	0.06
P-29	91	J-19	HYD-3	250.0	110.0	0.08
P-32	101	J-22	J-23	300.0	120.0	0.06
P-33	94	J-23	J-21	300.0	120.0	0.17
P-35	1	J-2	J-1	300.0	120.0	0.15
P-36	1	J-2	J-3	300.0	120.0	0.32
P-37	1	R-1	PMP-1	300.0	120.0	0.73
P-38	1	PMP-1	J-2	300.0	120.0	0.73

10242 Glendon Drive Subdivision

Water Age Analysis

Junction Table - Time: 0.00 hours

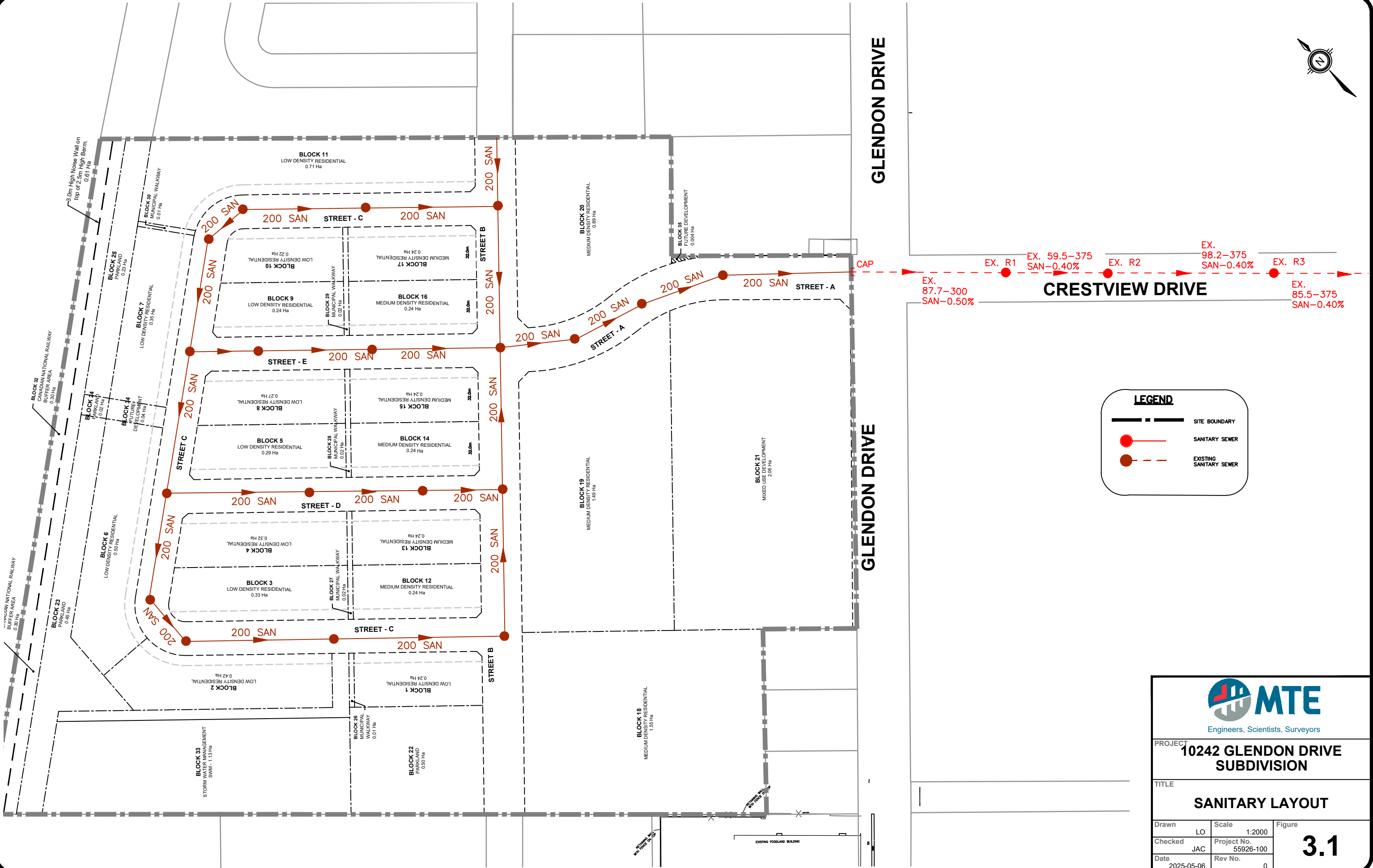
Label	Elevation (m)	Demand (L/s)	Hydraulic Grade (m)	Pressure (kPa)	Age (Maximum) (hours)	Block ID
HYD-1	247.87	0.00	281.47	329	0.548	
HYD-2	247.69	0.00	281.47	331	2.618	
HYD-3	248.02	0.00	281.47	327	2.374	
HYD-4	247.65	0.00	281.47	331	3.518	
HYD-5	246.84	0.00	281.46	339	4.486	
HYD-6	247.72	0.00	281.47	330	11.866	
HYD-7	249.22	0.00	281.47	316	10.602	
HYD-8	249.47	0.00	281.47	313	5.635	
HYD-9	249.90	0.00	281.47	309	4.290	
J-1	249.20	0.00	281.47	316	0.300	
J-2	247.18	0.00	281.47	336	0.200	
J-3	240.36	0.00	281.47	402	0.300	
J-4	241.04	4.21	281.47	396	0.664	
J-5	246.25	6.01	281.46	345	2.993	
J-6	246.96	0.00	281.47	338	4.363	
J-7	247.36	0.00	281.47	334	3.144	
J-10	248.20	0.00	281.47	326	2.187	
J-11	246.20	0.00	281.47	345	1.567	
J-12	249.74	0.28	281.47	311	5.872	
J-13	249.31	0.33	281.47	315	7.657	
J-15	248.73	0.36	281.47	320	8.940	
J-16	246.98	0.27	281.47	337	14.344	
J-17	248.79	0.36	281.47	320	4.990	
J-18	248.66	0.36	281.47	321	3.819	
J-19	249.20	0.28	281.47	316	3.373	
J-20	250.06	0.30	281.47	307	4.425	
J-21	248.24	0.66	281.47	325	0.731	
J-22	247.87	1.14	281.47	329	2.709	
J-23	248.28	2.62	281.47	325	1.202	

10242 Glendon Drive Subdivision
Water Age Analysis
Pipe Table - Time: 0.00 hours

Label	Length (m)	Start Node	Stop Node	Diameter (mm)	Hazen-Williams C	Velocity (m/s)
P-1	139	J-3	J-4	300.0	120.0	0.11
P-2	99	J-4	J-5	300.0	120.0	0.05
P-3	80	J-5	HYD-5	300.0	110.0	0.04
P-4	17	HYD-5	J-6	300.0	110.0	0.04
P-5	82	J-6	J-7	300.0	120.0	0.04
P-6	85	J-7	HYD-2	300.0	120.0	0.04
P-7	97	HYD-2	HYD-3	300.0	120.0	0.03
P-8	35	HYD-3	J-10	300.0	120.0	0.05
P-9	115	J-10	J-11	300.0	120.0	0.05
P-10	235	J-11	J-1	300.0	120.0	0.05
P-11	107	J-2	HYD-1	300.0	120.0	0.09
P-12	56	HYD-1	J-21	300.0	120.0	0.09
P-13	73	J-21	HYD-2	300.0	120.0	0.02
P-14	98	HYD-2	J-18	200.0	110.0	0.02
P-15	73	J-18	HYD-8	200.0	110.0	0.01
P-16	25	HYD-8	J-12	200.0	110.0	0.01
P-17	86	J-12	J-13	200.0	110.0	0.02
P-18	19	J-13	HYD-7	200.0	110.0	0.00
P-19	86	HYD-7	J-17	200.0	110.0	0.00
P-20	83	J-17	HYD-4	200.0	110.0	0.02
P-21	21	HYD-4	J-7	200.0	110.0	0.02
P-22	79	J-13	J-15	200.0	110.0	0.02
P-23	60	J-15	HYD-6	200.0	110.0	0.01
P-24	43	HYD-6	J-16	200.0	110.0	0.01
P-25	111	J-16	J-6	200.0	110.0	0.00
P-26	95	J-12	J-20	200.0	110.0	0.02
P-27	15	J-20	HYD-9	200.0	110.0	0.03
P-28	65	HYD-9	J-19	250.0	110.0	0.02
P-29	91	J-19	HYD-3	250.0	110.0	0.03
P-32	101	J-22	J-23	300.0	120.0	0.02
P-33	94	J-23	J-21	300.0	120.0	0.06
P-35	1	J-2	J-1	300.0	120.0	0.05
P-36	1	J-2	J-3	300.0	120.0	0.11
P-37	1	R-1	PMP-1	300.0	120.0	0.24
P-38	1	PMP-1	J-2	300.0	120.0	0.24

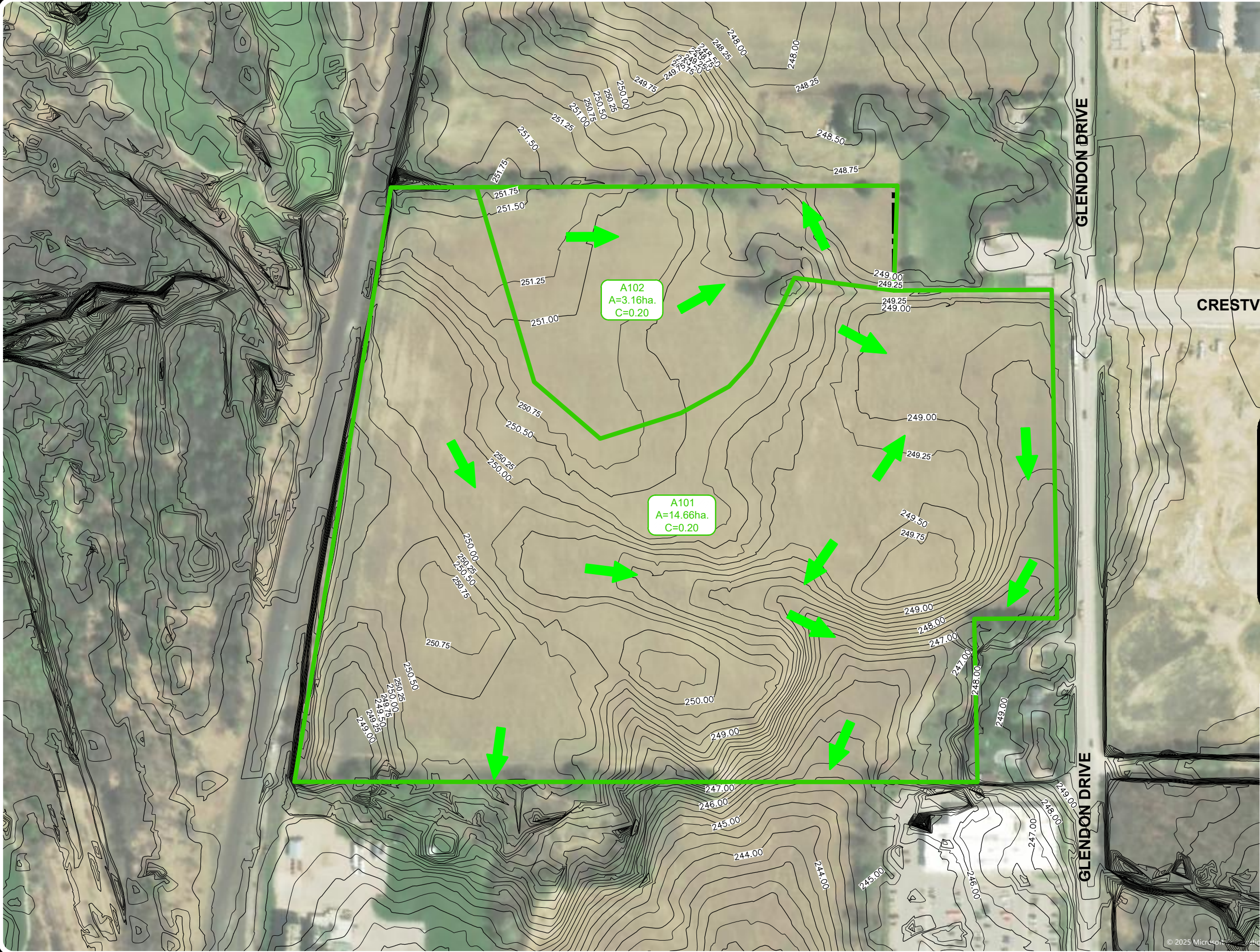
Appendix 2

Sanitary Servicing Information



Appendix 4

Stormwater Servicing Information



LEGEND

- SITE BOUNDARY
- STORM AREA
- DRAINAGE DIRECTION
- A101

A=0.68ha.

C=0.79

DRAINAGE ID

DRAINAGE AREA

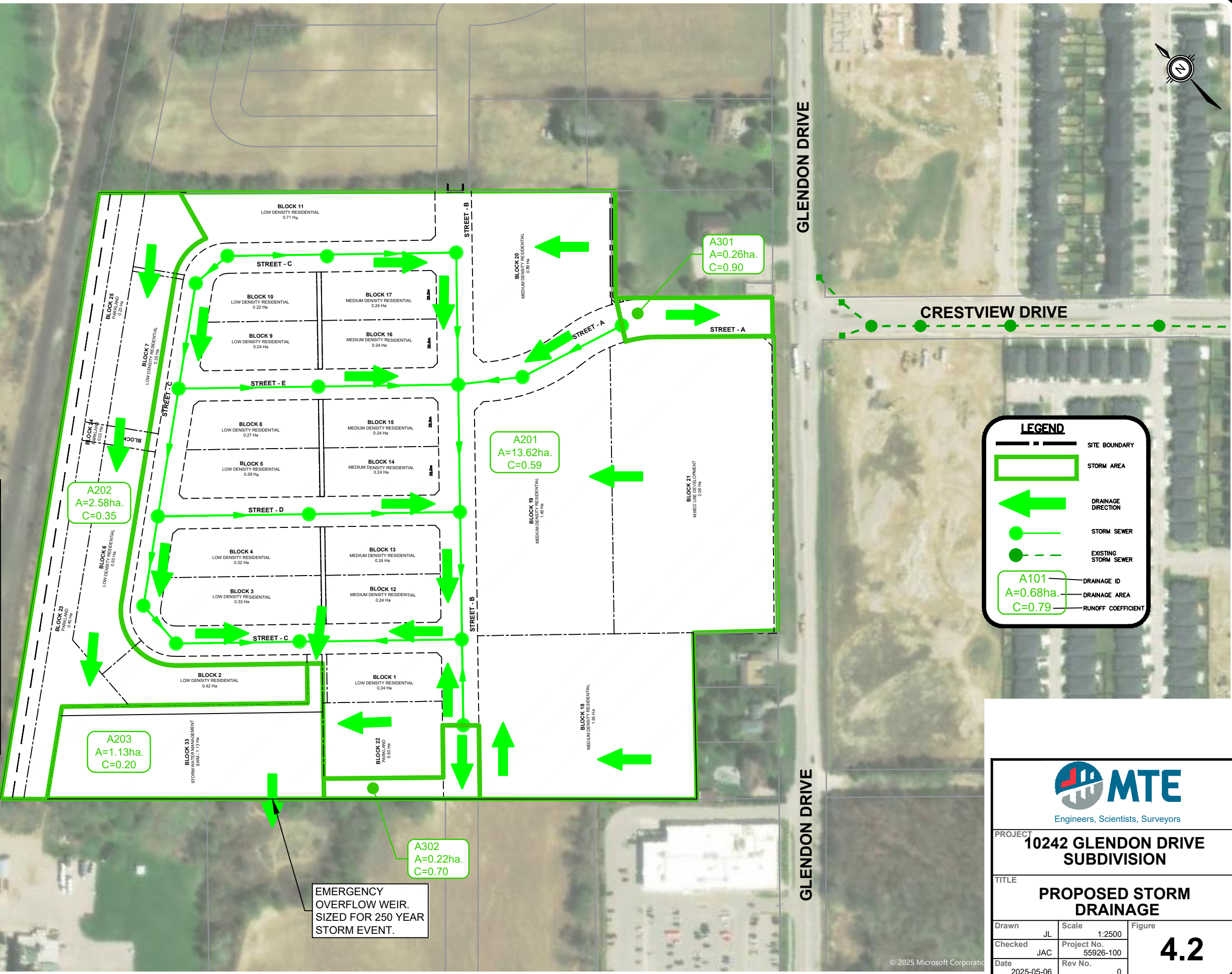
RUNOFF COEFFICIENT

Engineers, Scientists, Surveyors

PROJECT		
10242 GLENDON DRIVE SUBDIVISION		
TITLE		
EXISTING DRAINAGE		
Drawn	Scale	Figure
JL	1:2500	4.1
Checked	Project No.	
JAC	55926-100	
Date	Rev No.	
2025-05-06	0	

Area 1	Type	A	C	A* C
Block 22	P	0.5	0.20	0.1
Block 10	L	0.22	0.50	0.11
Block 9	L	0.24	0.50	0.12
Block 8	L	0.27	0.50	0.135
Block 5	L	0.29	0.50	0.145
Block 4	L	0.32	0.50	0.16
Block 3	L	0.33	0.50	0.165
Block 1	L	0.24	0.50	0.12
Block 11	L	0.54	0.50	0.269
Block 17	M	0.24	0.65	0.156
Block 16	M	0.24	0.65	0.156
Block 15	M	0.24	0.65	0.156
Block 14	M	0.24	0.65	0.156
Block 13	M	0.24	0.65	0.156
Block 12	M	0.24	0.65	0.156
Block 19	M	1.49	0.65	0.969
Block 21	M	2.06	0.65	1.339
Block 20	M	0.89	0.65	0.579
Block 18	M	1.55	0.65	1.008
Total Above		10.378		
Area Total		13.62		
Other		3.242		
	Grass	1.458	0.20	0.292
	Hard Surface	1.782	0.90	1.604
			A* C Total=	8.049
			Final C	0.59

Area 2	Type	A	C	A* C
Block 25	P	0.23	0.20	0.046
Block 24	P	0.02	0.20	0.004
Block 23	P	0.45	0.20	0.09
Block 2	L	0.24	0.50	0.12
Block 6	L	0.5	0.50	0.25
Block 7	L	0.35	0.50	0.175
Block 11	L	0.17	0.50	0.085
Block 34	L	0.04	0.50	0.02
Total Above		2		
Area Total		2.6		
Other				
	Grass	0.6	0.20	0.12
			A* C Total=	0.91
			Final C=	0.35



LEGEND

SITE BOUNDARY

STORM AREA

DRAINAGE DIRECTION

STORM SEWER

EXISTING STORM SEWER

A101
A=0.68ha.
C=0.79

DRAINAGE ID

DRAINAGE AREA

RUNOFF COEFFICIENT

MTE

Engineers, Scientists, Surveyors

PROJECT

10242 GLENDON DRIVE SUBDIVISION

TITLE

PROPOSED STORM DRAINAGE

Drawn

JL

Scale

1:2500

Figure

4.2

Checked

JAC

Project No.

55926-100

Date

2025-05-06

Rev No.

0



10242 Glendon Drive
STORMWATER MANAGEMENT
 Komoka, Ontario

Project Number: 55926-100
 Date: May 22, 2025
 Design By: JAC
 File: <https://mte85.sharepoint.com/sites/55926-100/Shared Documents/MTE Reports/FSR/swm/55926-100Master SWM Facility Design Sheet.xlsx>

HYDROLOGIC PARAMETERS

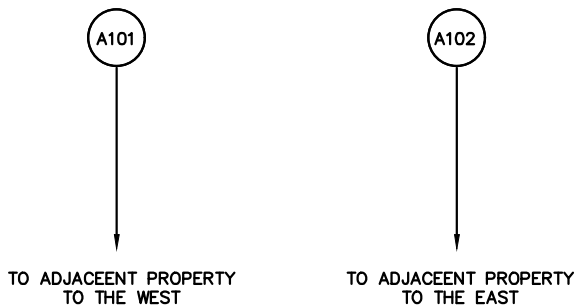
Pre-Development Conditions

Sub-Catchment Number	Area	Overland Slope	Overland Length	SCS Curve Number			Percent Impervious	Land Use	Comment
				Pervious (AMC II)	Pervious (AMC III)	Impervious			
	(ha)	(%)	(m)				(%)		
101	14.66	525	0.93	75	87	98	0	Agriculture	Drains Externaly
102	3.16	210	0.77	75	87	98	0	Agriculture	Drains Externaly
Total	17.82						0.00		

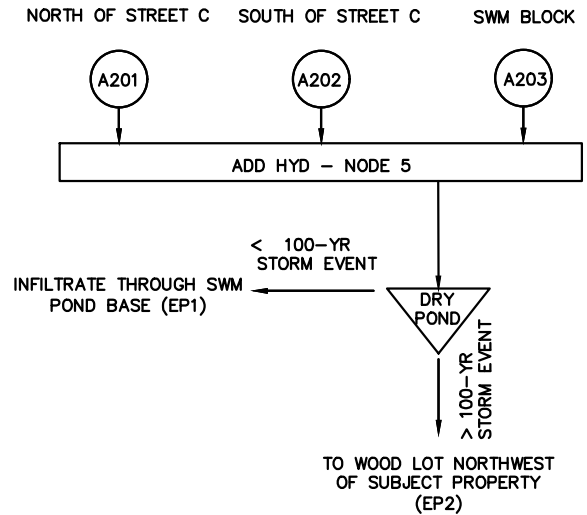
Post-Development Conditions

Sub-Catchment Number	Area	Overland Slope	Overland Length	SCS Curve Number			Percent Impervious	Land Use	Comment
				Pervious (AMC II)	Pervious (AMC III)	Impervious			
	(ha)	(%)	(m)				(%)		
201	13.62	2	356	75	87	98	52.1	Residential	Proposed Dev.
202	2.58	0.8	555	81	91	98	25	Residential	Proposed Dev.
203	1.13				0	98	0	SWM Pond	Proposed Dev.
301	0.26	2	57	95	98	98	45	Road	Proposed Dev.
302	0.22	1.8	105	95	98	98	45	Road	Proposed Dev.
Total	17.81						44.68		
Total to Pond	16.2						47.78		

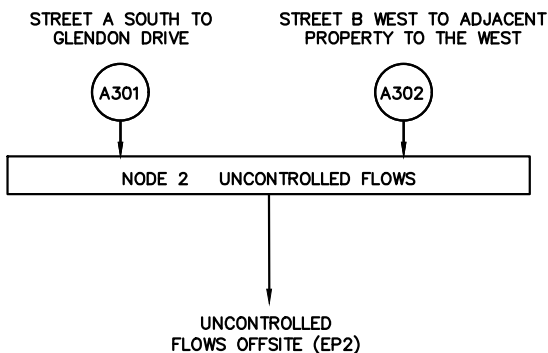
PRE-DEVELOPMENT HYDROLOGIC MODELLING SCHEMATIC



POST-DEVELOPMENT (CONTROLLED) HYDROLOGIC MODELLING SCHEMATIC



POST-DEVELOPMENT (UNCONTROLLED) HYDROLOGIC MODELLING SCHEMATIC



LEGEND

-  HYDROGRAPH GENERATION
-  HYDROGRAPH ROUTING
-  HYDROGRAPH ADDITION
MIDUSS STORAGE LOCATION NUMBER

FIGURE 4.3

Date: 5/20/2025
Scale: N/A

HYDROLOGIC MODELLING SCHEMATIC



Engineers | Scientists | Surveyors

Project No.: 55926-100

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SSSSS W W M M H H Y Y M M 000 999 999
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S W W W MM MM H H Y Y MM MM O O 9 9 9 9
SSSSS W W W M M M HHHHH Y M M M O O ## 9 9 9 9 Ver
4.05
S W W M M H H Y M M O O 9999 9999 Sept
2011
SSSSS W W M M H H Y M M 000 9 9
=====
9 9 9 9 #
3053466
StormWater Management HYdrologic Model 999 999
=====

```

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*****
*
***** SWMHYMO Ver/4.05
*****
***** A single event and continuous hydrologic simulation model
*****
***** based on the principles of HYMO and its successors
*****
***** OTTHYMO-83 and OTTHYMO-89.
*****

```

```

*****
*
***** Distributed by: J.F. Sabourin and Associates Inc.
*****
***** Ottawa, Ontario: (613) 836-3884
*****
***** Gatineau, Quebec: (819) 243-6858
*****
***** E-Mail: swmhymo@jfsa.Com
*****

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+++++
+
+++++ Licensed user: MTE Consultants Inc.
+++++
+++++ Burlington SERIAL#:3053466
+++++
+++++
+

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*****
*
*****
++++++ PROGRAM ARRAY DIMENSIONS ++++++
*****
*****
Maximum value for ID numbers : 10
*****
*****
Max. number of rainfall points: 105408
*****
*****
Max. number of flow points : 105408
*****

*****
*

*****
D E T A I L E D O U T P U T
*****

*****
*
* DATE: 2025-05-21 TIME: 13:12:50 RUN COUNTER: 000009
*

*****
*
* Input filename: Q:\55926\100\202505~1\SWMHYMO\PREMODEL.dat
*
* Output filename: Q:\55926\100\202505~1\SWMHYMO\PREMODEL.out
*
* Summary filename: Q:\55926\100\202505~1\SWMHYMO\PREMODEL.sum
*
* User comments:
*
*
1: _____*
*
2: _____*
*
3: _____*

*****
*

-----
-----
001:0001-----
-----
*#*****
**
*# Project Name: [GLENDON] Project Number: [55926-100]

```


*# Date : OCTOBER 2024
*# Modeller : [JJM]
*# Company : MTE CONSULTANTS INC.
*# License # :

**

| START | Project dir.: Q:\55926\100\202505~1\SWMHYMO\

----- Rainfall dir.: Q:\55926\100\202505~1\SWMHYMO\

TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 001
NSTORM= 1
1=25mm.HYT

001:0002-----

| READ STORM | Filename: 25mm Chicago 4-hr duration
| Ptotal= 24.83 mm | Comments: 25mm Chicago 4-hr duration

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	1.326	1.17	3.978	2.25	4.889	3.33	1.844
.17	1.392	1.25	4.803	2.33	4.304	3.42	1.765
.25	1.466	1.33	6.089	2.42	3.849	3.50	1.693
.33	1.549	1.42	8.350	2.50	3.485	3.58	1.627
.42	1.643	1.50	13.259	2.58	3.187	3.67	1.567
.50	1.750	1.58	29.925	2.67	2.939	3.75	1.511
.58	1.875	1.67	75.600	2.75	2.729	3.83	1.460
.67	2.020	1.75	27.475	2.83	2.549	3.92	1.412
.75	2.193	1.83	15.856	2.92	2.392	4.00	1.368
.83	2.401	1.92	10.977	3.00	2.256	4.08	1.326
.92	2.657	2.00	8.363	3.08	2.135		
1.00	2.981	2.08	6.752	3.17	2.027		
1.08	3.404	2.17	5.667	3.25	1.930		

001:0003-----

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* AREAS TRIBUTARY TO THE WEST

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*EXISTING AGRICULTURAL LANDS (WEST)

*=====

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CALIB NASHYD		Area (ha)=	14.66	Curve Number (CN)=75.00
01:101 DT= 5.00		Ia (mm)=	5.000	# of Linear Res.(N)= 3.00
-----		U.H. Tp(hrs)=	.690	

Unit Hyd Qpeak (cms)= .812

PEAK FLOW (cms)= .076 (i)

TIME TO PEAK (hrs)= 2.583

RUNOFF VOLUME (mm)= 3.764

TOTAL RAINFALL (mm)= 24.833

RUNOFF COEFFICIENT = .152

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0004-----

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* AREAS TRIBUTARY TO THE EAST

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*EXISTING AGRICULTURAL LANDS (EAST)

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=

CALIB NASHYD		Area (ha)=	3.16	Curve Number (CN)=75.00
02:102 DT= 5.00		Ia (mm)=	5.000	# of Linear Res.(N)= 3.00
-----		U.H. Tp(hrs)=	.460	

Unit Hyd Qpeak (cms)= .262

PEAK FLOW (cms)= .021 (i)
TIME TO PEAK (hrs)= 2.250
RUNOFF VOLUME (mm)= 3.764
TOTAL RAINFALL (mm)= 24.833
RUNOFF COEFFICIENT = .152

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0005-----

** END OF RUN : 1

*

| START | Project dir.: Q:\55926\100\202505~1\SWMHYMO\

----- Rainfall dir.: Q:\55926\100\202505~1\SWMHYMO\

TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 002
NSTORM= 1
1=2YR.HYT

002:0002-----

*#*****
**

*# Project Name: [GLENDON] Project Number: [55926-100]

*# Date : OCTOBER 2024

*# Modeller : [JJM]

*# Company : MTE CONSULTANTS INC.

*# License # :

*#*****
**

002:0002-----

READ STORM	Filename: 2YR Chicago 3-hr duration
Ptotal= 32.95 mm	Comments: 2YR Chicago 3-hr duration

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	2.366	.92	7.556	1.75	8.343	2.58	3.173
.17	2.528	1.00	9.957	1.83	7.120	2.67	2.999
.25	2.716	1.08	14.640	1.92	6.218	2.75	2.844
.33	2.938	1.17	27.128	2.00	5.527	2.83	2.706
.42	3.203	1.25	106.663	2.08	4.980	2.92	2.581
.50	3.527	1.33	54.508	2.17	4.537	3.00	2.469
.58	3.931	1.42	26.925	2.25	4.170	3.08	2.366
.67	4.449	1.50	17.418	2.33	3.862		
.75	5.140	1.58	12.788	2.42	3.599		
.83	6.108	1.67	10.093	2.50	3.372		

002:0003-

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* AREAS TRIBUTARY TO THE WEST

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*EXISTING AGRICULTURAL LANDS (WEST)

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CALIB NASHYD	Area	(ha)=	14.66	Curve Number	(CN)=75.00
01:101 DT= 5.00	Ia	(mm)=	5.000	# of Linear Res.(N)=	3.00
-----	U.H. Tp(hrs)=		.690		

Unit Hyd Qpeak (cms)= .812

PEAK FLOW (cms)= .156 (i)

TIME TO PEAK (hrs)= 2.167

RUNOFF VOLUME (mm)= 6.938

TOTAL RAINFALL (mm)= 32.954

RUNOFF COEFFICIENT = .211

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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002:0004-----
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*          AREAS TRIBUTARY TO THE EAST

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=
*EXISTING AGRICULTURAL LANDS (EAST)

*=====
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-----
| CALIB NASHYD      | Area   (ha)=   3.16   Curve Number   (CN)=75.00
| 02:102   DT= 5.00 | Ia     (mm)=   5.000   # of Linear Res.(N)= 3.00
-----
                        U.H. Tp(hrs)=   .460

      Unit Hyd Qpeak  (cms)=   .262

      PEAK FLOW        (cms)=   .044 (i)
      TIME TO PEAK     (hrs)=   1.833
      RUNOFF VOLUME    (mm)=   6.938
      TOTAL RAINFALL   (mm)=  32.954
      RUNOFF COEFFICIENT =   .211

      (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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-----
002:0005-----
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002:0002-----
-----
** END OF RUN :    4

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*

-----
| START              | Project  dir.: Q:\55926\100\202505~1\SWMHYMO\

```

----- Rainfall dir.: Q:\55926\100\202505~1\SWMHYMO\

TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 005
NSTORM= 1
1=5YR.HYT

005:0002-----

**

*# Project Name: [GLENDON] Project Number: [55926-100]

*# Date : OCTOBER 2024

*# Modeller : [JJM]

*# Company : MTE CONSULTANTS INC.

*# License # :

**

005:0002-----

| READ STORM | Filename: 5YR Chicago 3-hr duration
| Ptotal= 44.47 mm | Comments: 5YR Chicago 3-hr duration

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	2.889	.92	10.155	1.75	11.292	2.58	3.967
.17	3.102	1.00	13.656	1.83	9.520	2.67	3.731
.25	3.352	1.08	20.548	1.92	8.224	2.75	3.523
.33	3.649	1.17	38.765	2.00	7.239	2.83	3.338
.42	4.007	1.25	141.200	2.08	6.466	2.92	3.173
.50	4.447	1.33	76.415	2.17	5.844	3.00	3.024
.58	5.002	1.42	38.412	2.25	5.333	3.08	2.889
.67	5.722	1.50	24.610	2.33	4.907		
.75	6.693	1.58	17.806	2.42	4.545		
.83	8.068	1.67	13.848	2.50	4.235		

005:0003-----

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* AREAS TRIBUTARY TO THE WEST

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*EXISTING AGRICULTURAL LANDS (WEST)

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=

CALIB NASHYD		Area	(ha)=	14.66	Curve Number	(CN)=75.00
01:101 DT= 5.00		Ia	(mm)=	5.000	# of Linear Res.(N)=	3.00
-----		U.H. Tp(hrs)=		.690		

Unit Hyd Qpeak (cms)= .812

PEAK FLOW (cms)= .293 (i)

TIME TO PEAK (hrs)= 2.167

RUNOFF VOLUME (mm)= 12.548

TOTAL RAINFALL (mm)= 44.466

RUNOFF COEFFICIENT = .282

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0004-----

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* AREAS TRIBUTARY TO THE EAST

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*EXISTING AGRICULTURAL LANDS (EAST)

*=====

=

CALIB NASHYD		Area	(ha)=	3.16	Curve Number	(CN)=75.00
02:102 DT= 5.00		Ia	(mm)=	5.000	# of Linear Res.(N)=	3.00
-----		U.H. Tp(hrs)=		.460		

Unit Hyd Qpeak (cms)= .262
PEAK FLOW (cms)= .084 (i)
TIME TO PEAK (hrs)= 1.833
RUNOFF VOLUME (mm)= 12.548
TOTAL RAINFALL (mm)= 44.466
RUNOFF COEFFICIENT = .282

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0005-----

005:0002-----

005:0002-----

** END OF RUN : 9

*

| START | Project dir.: Q:\55926\100\202505~1\SWMHYMO\

Rainfall dir.: Q:\55926\100\202505~1\SWMHYMO\

TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 010
NSTORM= 1
1=10YR.HYT

010:0002-----

**
**
** Project Name: [GLENDON] Project Number: [55926-100]
** Date : OCTOBER 2024
** Modeller : [JJM]

*# Company : MTE CONSULTANTS INC.

*# License # :

*#*****
**

010:0002-----

| READ STORM | Filename: 10YR Chicago 3-hr duration
| Ptotal= 52.37 mm | Comments: 10YR Chicago 3-hr duration

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	3.141	.92	11.986	1.75	13.417	2.58	4.407
.17	3.389	1.00	16.365	1.83	11.203	2.67	4.128
.25	3.681	1.08	25.006	1.92	9.593	2.75	3.882
.33	4.030	1.17	47.536	2.00	8.375	2.83	3.665
.42	4.454	1.25	162.500	2.08	7.426	2.92	3.472
.50	4.979	1.33	92.425	2.17	6.667	3.00	3.298
.58	5.645	1.42	47.240	2.25	6.047	3.08	3.141
.67	6.517	1.50	30.137	2.33	5.531		
.75	7.701	1.58	21.600	2.42	5.097		
.83	9.394	1.67	16.623	2.50	4.727		

010:0003-----

*=====

* AREAS TRIBUTARY TO THE WEST

*=====

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*=====

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*EXISTING AGRICULTURAL LANDS (WEST)

*=====

=

| CALIB NASHYD | Area (ha)= 14.66 Curve Number (CN)=75.00
| 01:101 DT= 5.00 | Ia (mm)= 5.000 # of Linear Res.(N)= 3.00

U.H. Tp(hrs)= .690

Unit Hyd Qpeak (cms)= .812

PEAK FLOW (cms)= .404 (i)
TIME TO PEAK (hrs)= 2.083
RUNOFF VOLUME (mm)= 16.994
TOTAL RAINFALL (mm)= 52.369
RUNOFF COEFFICIENT = .325

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0004-----

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* AREAS TRIBUTARY TO THE EAST

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*EXISTING AGRICULTURAL LANDS (EAST)

*=====

=

| CALIB NASHYD | Area (ha)= 3.16 Curve Number (CN)=75.00
| 02:102 DT= 5.00 | Ia (mm)= 5.000 # of Linear Res.(N)= 3.00
----- U.H. Tp(hrs)= .460

Unit Hyd Qpeak (cms)= .262

PEAK FLOW (cms)= .117 (i)
TIME TO PEAK (hrs)= 1.833
RUNOFF VOLUME (mm)= 16.994
TOTAL RAINFALL (mm)= 52.369
RUNOFF COEFFICIENT = .325

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0005-----

010:0002-----

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010:0002-----
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-----
-----
010:0002-----
-----
** END OF RUN : 24

*****
*

-----
| START          | Project dir.: Q:\55926\100\202505~1\SWMHYMO\
-----
Rainfall dir.: Q:\55926\100\202505~1\SWMHYMO\

    TZERO = .00 hrs on      0
    METOUT= 2 (output = METRIC)
    NRUN  = 025
    NSTORM= 1
           # 1=25YR.HYT
-----
-----
025:0002-----
-----
*#*****
**
*# Project Name: [GLENDON]    Project Number: [55926-100]

*# Date           : OCTOBER 2024

*# Modeller       : [JJM]

*# Company        : MTE CONSULTANTS INC.

*# License #      :

*#*****
**

-----
-----
025:0002-----
-----
-----
| READ STORM      | Filename: 25YR Chicago 3-hr duration
| Ptotal= 61.85 mm| Comments: 25YR Chicago 3-hr duration
-----

```

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	3.490	.92	14.107	1.75	15.861	2.58	4.972
.17	3.779	1.00	19.457	1.83	13.158	2.67	4.644
.25	4.120	1.08	30.035	1.92	11.200	2.75	4.356
.33	4.529	1.17	57.437	2.00	9.725	2.83	4.101
.42	5.028	1.25	190.801	2.08	8.578	2.92	3.875
.50	5.649	1.33	111.064	2.17	7.665	3.00	3.672
.58	6.442	1.42	57.174	2.25	6.922	3.08	3.490
.67	7.484	1.50	36.348	2.33	6.307		
.75	8.908	1.58	25.889	2.42	5.790		
.83	10.956	1.67	19.786	2.50	5.351		

025:0003-

AREAS TRIBUTARY TO THE WEST

*EXISTING AGRICULTURAL LANDS (WEST)

CALIB NASHYD	Area	(ha)=	14.66	Curve Number	(CN)=75.00
01:101 DT= 5.00	Ia	(mm)=	5.000	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=		.690		

Unit Hyd Qpeak (cms)= .812

PEAK FLOW (cms)= .553 (i)

TIME TO PEAK (hrs)= 2.083

RUNOFF VOLUME (mm)= 22.835

TOTAL RAINFALL (mm)= 61.846

RUNOFF COEFFICIENT = .369

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0004-

=
*

* AREAS TRIBUTARY TO THE EAST

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*=====

*EXISTING AGRICULTURAL LANDS (EAST)

*=====

CALIB NASHYD		Area	(ha)=	3.16
02:102 DT= 5.00		Ia	(mm)=	5.000
-----		U.H. Tp(hrs)=		.460

Unit Hyd Qpeak (cms)= .262

PEAK FLOW (cms)= .160 (i)

TIME TO PEAK (hrs)= 1.833

RUNOFF VOLUME (mm)= 22.835

TOTAL RAINFALL (mm)= 61.846

RUNOFF COEFFICIENT = .369

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0005-----

025:0002-----

025:0002-----

025:0002-----

025:0002-----

** END OF RUN : 49

*

```
-----
| START          | Project dir.: Q:\55926\100\202505~1\SWMHYMO\
----- Rainfall dir.: Q:\55926\100\202505~1\SWMHYMO\

TZERO = .00 hrs on      0
METOUT= 2 (output = METRIC)
NRUN   = 050
NSTORM= 1
      # 1=50YR.HYT
-----
-----
050:0002-----
-----
**#*****
**
*# Project Name: [GLENDON]    Project Number: [55926-100]

*# Date           : OCTOBER 2024

*# Modeller       : [JJM]

*# Company        : MTE CONSULTANTS INC.

*# License #      :

**#*****
**
-----
-----
050:0002-----
-----
-----
| READ STORM      | Filename: 50YR Chicago 3-hr duration
| Ptotal= 69.13 mm| Comments: 50YR Chicago 3-hr duration
-----

```

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	3.895	.92	15.824	1.75	17.797	2.58	5.558
.17	4.219	1.00	21.837	1.83	14.758	2.67	5.189
.25	4.601	1.08	33.713	1.92	12.556	2.75	4.866
.33	5.060	1.17	64.387	2.00	10.897	2.83	4.580
.42	5.620	1.25	212.001	2.08	9.609	2.92	4.326
.50	6.318	1.33	124.085	2.17	8.582	3.00	4.100
.58	7.208	1.42	64.104	2.25	7.747	3.08	3.895
.67	8.379	1.50	40.797	2.33	7.057		
.75	9.980	1.58	29.062	2.42	6.476		

.83 12.281 | 1.67 22.208 | 2.50 5.983 |

050:0003

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* AREAS TRIBUTARY TO THE WEST

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*EXISTING AGRICULTURAL LANDS (WEST)

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CALIB NASHYD		Area	(ha)=	14.66	Curve Number	(CN)=75.00
01:101 DT= 5.00		Ia	(mm)=	5.000	# of Linear Res.(N)=	3.00
-----		U.H. Tp(hrs)=		.690		

Unit Hyd Qpeak (cms)= .812

PEAK FLOW (cms)= .672 (i)

TIME TO PEAK (hrs)= 2.083

RUNOFF VOLUME (mm)= 27.639

TOTAL RAINFALL (mm)= 69.130

RUNOFF COEFFICIENT = .400

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

050:0004

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* AREAS TRIBUTARY TO THE EAST

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*EXISTING AGRICULTURAL LANDS (EAST)

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-----
| CALIB NASHYD      | Area   (ha)=   3.16   Curve Number   (CN)=75.00
| 02:102    DT= 5.00 | Ia     (mm)=   5.000   # of Linear Res.(N)= 3.00
-----
                        U.H. Tp(hrs)=   .460
```

Unit Hyd Qpeak (cms)= .262

PEAK FLOW (cms)= .195 (i)

TIME TO PEAK (hrs)= 1.833

RUNOFF VOLUME (mm)= 27.639

TOTAL RAINFALL (mm)= 69.130

RUNOFF COEFFICIENT = .400

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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050:0005-----
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050:0002-----
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050:0002-----
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050:0002-----
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050:0002-----
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050:0002-----
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** END OF RUN : 99

*

| START | Project dir.: Q:\55926\100\202505~1\SWMHYMO\

----- Rainfall dir.: Q:\55926\100\202505~1\SWMHYMO\

TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 100
NSTORM= 1
1=100YR.HYT

100:0002-----

*#*****

**

*# Project Name: [GLENDON] Project Number: [55926-100]

*# Date : OCTOBER 2024

*# Modeller : [JJM]

*# Company : MTE CONSULTANTS INC.

*# License # :

*#*****

**

100:0002-----

| READ STORM | Filename: 100YR Chicago 3-hr duration
| Ptotal= 76.27 mm | Comments: 100YR Chicago 3-hr duration

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	4.164	.92	17.483	1.75	19.709	2.58	5.997
.17	4.519	1.00	24.251	1.83	16.288	2.67	5.589
.25	4.940	1.08	37.617	1.92	13.813	2.75	5.232
.33	5.447	1.17	71.935	2.00	11.952	2.83	4.917
.42	6.066	1.25	232.200	2.08	10.509	2.92	4.638
.50	6.839	1.33	137.906	2.17	9.361	3.00	4.388
.58	7.828	1.42	71.694	2.25	8.430	3.08	4.164
.67	9.133	1.50	45.604	2.33	7.661		
.75	10.922	1.58	32.403	2.42	7.015		
.83	13.502	1.67	24.679	2.50	6.467		

100:0003-----

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* AREAS TRIBUTARY TO THE WEST

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*EXISTING AGRICULTURAL LANDS (WEST)

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CALIB NASHYD		Area	(ha)=	14.66	Curve Number (CN)=75.00
01:101 DT= 5.00		Ia	(mm)=	5.000	# of Linear Res.(N)= 3.00
-----		U.H.	Tp(hrs)=	.690	

Unit Hyd Qpeak (cms)= .812

PEAK FLOW (cms)= .798 (i)

TIME TO PEAK (hrs)= 2.083

RUNOFF VOLUME (mm)= 32.575

TOTAL RAINFALL (mm)= 76.272

RUNOFF COEFFICIENT = .427

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0004-----

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* AREAS TRIBUTARY TO THE EAST

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*EXISTING AGRICULTURAL LANDS (EAST)

*=====

=

CALIB NASHYD		Area	(ha)=	3.16	Curve Number (CN)=75.00
02:102 DT= 5.00		Ia	(mm)=	5.000	# of Linear Res.(N)= 3.00

----- U.H. Tp(hrs)= .460

Unit Hyd Qpeak (cms)= .262

PEAK FLOW (cms)= .232 (i)

TIME TO PEAK (hrs)= 1.833

RUNOFF VOLUME (mm)= 32.575

TOTAL RAINFALL (mm)= 76.272

RUNOFF COEFFICIENT = .427

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0005-----

100:0002-----

100:0002-----

100:0002-----

100:0002-----

100:0002-----

100:0002-----

FINISH

WARNINGS / ERRORS / NOTES

Simulation ended on 2025-05-21 at 13:12:52

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SSSSS W W M M H H Y Y M M 000 999 999
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S W W W MM MM H H Y Y MM MM O O 9 9 9 9
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4.05
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2011
SSSSS W W M M H H Y M M 000 9 9
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9 9 9 9 #
3053466
StormWater Management HYdrologic Model 999 999
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*****
*
***** SWMHYMO Ver/4.05
*****
***** A single event and continuous hydrologic simulation model
*****
***** based on the principles of HYMO and its successors
*****
***** OTTHYMO-83 and OTTHYMO-89.
*****

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*****
*
***** Distributed by: J.F. Sabourin and Associates Inc.
*****
***** Ottawa, Ontario: (613) 836-3884
*****
***** Gatineau, Quebec: (819) 243-6858
*****
***** E-Mail: swmhymo@jfsa.Com
*****

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+++++
+
+++++ Licensed user: MTE Consultants Inc.
+++++
+++++ Burlington SERIAL#:3053466
+++++
+++++
+

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*****
*
* *****
*          ++++++ PROGRAM ARRAY DIMENSIONS ++++++
* *****
* *****
*          Maximum value for ID numbers   :    10
* *****
* *****
*          Max. number of rainfall points: 105408
* *****
* *****
*          Max. number of flow points     : 105408
* *****
```

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***** D E T A I L E D   O U T P U T *****
*****
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*****
*
*          DATE: 2025-05-27      TIME: 13:13:22      RUN COUNTER: 000033
*
```

```
*****
*
* Input   filename: Q:\55926\100\202505~1\SWMHYMO\POST_DEV.dat
*
* Output  filename: Q:\55926\100\202505~1\SWMHYMO\POST_DEV.out
*
* Summary filename: Q:\55926\100\202505~1\SWMHYMO\POST_DEV.sum
*
* User comments:
```

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1: _____*
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2: _____*
*
3: _____*
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001:0001-----
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```
*#*****
**
*# Project Name: [GLENDON ROAD]      Project Number: [55926-100]
```


*# Date : OCTOBER 2024
*# Modeller : [JJM]
*# Company : MTE CONSULTANTS INC.
*# License # :

**

| START | Project dir.: Q:\55926\100\202505~1\SWMHYMO\

----- Rainfall dir.: Q:\55926\100\202505~1\SWMHYMO\

TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 001
NSTORM= 1
1=25mm.HYT

001:0002-----

| READ STORM | Filename: 25mm Chicago 4-hr duration
| Ptotal= 24.83 mm | Comments: 25mm Chicago 4-hr duration

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	1.326	1.17	3.978	2.25	4.889	3.33	1.844
.17	1.392	1.25	4.803	2.33	4.304	3.42	1.765
.25	1.466	1.33	6.089	2.42	3.849	3.50	1.693
.33	1.549	1.42	8.350	2.50	3.485	3.58	1.627
.42	1.643	1.50	13.259	2.58	3.187	3.67	1.567
.50	1.750	1.58	29.925	2.67	2.939	3.75	1.511
.58	1.875	1.67	75.600	2.75	2.729	3.83	1.460
.67	2.020	1.75	27.475	2.83	2.549	3.92	1.412
.75	2.193	1.83	15.856	2.92	2.392	4.00	1.368
.83	2.401	1.92	10.977	3.00	2.256	4.08	1.326
.92	2.657	2.00	8.363	3.08	2.135		
1.00	2.981	2.08	6.752	3.17	2.027		
1.08	3.404	2.17	5.667	3.25	1.930		

001:0003-----

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* TRIBUTARY AREAS TO THE SOUTH OF STREET C

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CALIB STANDHYD	Area (ha)=	13.62		
01:201 DT= 2.00	Total Imp(%)=	62.00	Dir. Conn.(%)=	56.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	8.44	5.18	
Dep. Storage (mm)=	2.00	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	520.00	25.00	
Mannings n =	.015	.250	
Max.eff.Inten.(mm/hr)=	60.38	8.87	
over (min)	7.50	22.50	
Storage Coeff. (min)=	7.44 (ii)	21.47 (ii)	
Unit Hyd. Tpeak (min)=	7.50	22.50	
Unit Hyd. peak (cms)=	.15	.05	
			TOTALS
PEAK FLOW (cms)=	.90	.07	.926 (iii)
TIME TO PEAK (hrs)=	1.75	2.08	1.750
RUNOFF VOLUME (mm)=	22.83	5.58	15.244
TOTAL RAINFALL (mm)=	24.83	24.83	24.833
RUNOFF COEFFICIENT =	.92	.22	.614

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:

CN* = 80.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0004-

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* TRIBUTARY AREAS TO THE NORTH OF STREET C

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CALIB STANDHYD	Area (ha)=	2.58		
02:202 DT= 2.00	Total Imp(%)=	25.00	Dir. Conn.(%)=	22.50

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	.64	1.93	
Dep. Storage (mm)=	2.00	5.00	
Average Slope (%)=	.80	2.00	
Length (m)=	331.00	25.00	
Mannings n =	.015	.250	
Max.eff.Inten.(mm/hr)=	60.38	7.24	
over (min)	7.50	22.50	

Storage Coeff. (min)=	7.47 (ii)	22.69 (ii)	
Unit Hyd. Tpeak (min)=	7.50	22.50	
Unit Hyd. peak (cms)=	.15	.05	
			TOTALS
PEAK FLOW (cms)=	.07	.02	.075 (iii)
TIME TO PEAK (hrs)=	1.75	2.08	1.750
RUNOFF VOLUME (mm)=	22.83	5.15	9.127
TOTAL RAINFALL (mm)=	24.83	24.83	24.833
RUNOFF COEFFICIENT =	.92	.21	.368

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 81.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 001:0005-----

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* TRIBUTARY AREAS TO SWM POND

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CALIB NASHYD		Area (ha)=	1.13	Curve Number (CN)=75.00
03:203 DT= 2.00		Ia (mm)=	5.000	# of Linear Res.(N)= 3.00
-----		U.H. Tp(hrs)=	.180	

Unit Hyd Qpeak (cms)=	.240
PEAK FLOW (cms)=	.014 (i)
TIME TO PEAK (hrs)=	1.875
RUNOFF VOLUME (mm)=	3.764
TOTAL RAINFALL (mm)=	24.833
RUNOFF COEFFICIENT =	.152

- (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 001:0006-----

ADD HYD (	9)	ID: NHYD	AREA	QPEAK	TPEAK	R.V.	DWF
-----			(ha)	(cms)	(hrs)	(mm)	
(cms)							
		ID1 01:201	13.62	.926	1.75	15.24	
.000		+ID2 02:202	2.58	.075	1.75	9.13	
.000							

```

+ID3 03:203          1.13    .014    1.88    3.76
.000

=====
SUM 04:              9    17.33    1.011    1.75    13.58
.000

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NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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001:0007-----
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*ROUTE RUNOFF THROUGH PROPOSED POND
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-----
| ROUTE RESERVOIR | Requested routing time step = 2.0 min.
| IN>04:(000009) |
| OUT<05:(000204) |
-----
===== OUTFLOW STORAGE TABLE =====
OUTFLOW    STORAGE    | OUTFLOW    STORAGE
(cms)      (ha.m.)    | (cms)      (ha.m.)
.000    .0000E+00    | .026    .1010E+01
.026    .3121E-01    | .000    .0000E+00

```

ROUTING RESULTS	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW >04: (000009)	17.33	1.011	1.750	13.585
OUTFLOW<05: (000204)	17.33	.026	1.667	13.585
OVERFLOW<06: (000205)	.00	.000	.000	.000

```

TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
CUMULATIVE TIME OF OVERFLOWS (hours)= .00
PERCENTAGE OF TIME OVERFLOWING (%)= .00

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PEAK FLOW REDUCTION [Qout/Qin](%)= 2.572
TIME SHIFT OF PEAK FLOW (min)= -5.00
MAXIMUM STORAGE USED (ha.m.)=.2068E+00

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001:0008-----
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** END OF RUN : 1

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-----
| START          | Project dir.: Q:\55926\100\202505~1\SWMHYMO\
-----
Rainfall dir.: Q:\55926\100\202505~1\SWMHYMO\

TZERO = .00 hrs on      0
METOUT= 2 (output = METRIC)
NRUN   = 002
NSTORM= 1
      # 1=2YR.HYT
-----

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002:0002-----
-----
**#*****
**
*# Project Name: [GLENDON ROAD]   Project Number: [55926-100]

*# Date           : OCTOBER 2024

*# Modeller       : [JJM]

*# Company        : MTE CONSULTANTS INC.

*# License #      :

**#*****
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-----
002:0002-----
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-----
| READ STORM      | Filename: 2YR Chicago 3-hr duration
| Ptotal= 32.95 mm| Comments: 2YR Chicago 3-hr duration
-----


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TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	2.366	.92	7.556	1.75	8.343	2.58	3.173
.17	2.528	1.00	9.957	1.83	7.120	2.67	2.999
.25	2.716	1.08	14.640	1.92	6.218	2.75	2.844
.33	2.938	1.17	27.128	2.00	5.527	2.83	2.706
.42	3.203	1.25	106.663	2.08	4.980	2.92	2.581
.50	3.527	1.33	54.508	2.17	4.537	3.00	2.469
.58	3.931	1.42	26.925	2.25	4.170	3.08	2.366
.67	4.449	1.50	17.418	2.33	3.862		
.75	5.140	1.58	12.788	2.42	3.599		
.83	6.108	1.67	10.093	2.50	3.372		

002:0003

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* TRIBUTARY AREAS TO THE SOUTH OF STREET C

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CALIB STANDHYD	Area (ha)=	13.62		
01:201 DT= 2.00	Total Imp(%)=	62.00	Dir. Conn.(%)=	56.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	8.44	5.18
Dep. Storage	(mm)=	2.00	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	520.00	25.00
Mannings n	=	.015	.250

Max.eff.Inten.(mm/hr)=	106.66	22.34
over (min)	5.00	15.00
Storage Coeff. (min)=	5.93 (ii)	15.62 (ii)
Unit Hyd. Tpeak (min)=	5.00	15.00
Unit Hyd. peak (cms)=	.20	.07

			TOTALS
PEAK FLOW	(cms)=	1.43	.18
TIME TO PEAK	(hrs)=	1.29	1.54
RUNOFF VOLUME	(mm)=	30.95	9.82
TOTAL RAINFALL	(mm)=	32.95	32.95
RUNOFF COEFFICIENT	=	.94	.30

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 80.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0004

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* TRIBUTARY AREAS TO THE NORTH OF STREET C

*=====

=

CALIB STANDHYD	Area (ha)=	2.58		
02:202 DT= 2.00	Total Imp(%)=	25.00	Dir. Conn.(%)=	22.50

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-----
                IMPERVIOUS      PERVIOUS (i)
Surface Area    (ha)=          .64          1.93
Dep. Storage    (mm)=          2.00          5.00
Average Slope   (%)=          .80          2.00
Length          (m)=        331.00        25.00
Mannings n      =          .015          .250

Max.eff.Inten.(mm/hr)=      106.66          16.99
                    over (min)          5.00          17.50
Storage Coeff.  (min)=          5.95 (ii)    16.76 (ii)
Unit Hyd. Tpeak (min)=          5.00          17.50
Unit Hyd. peak  (cms)=          .20          .07

PEAK FLOW        (cms)=          .11          .05          .120 (iii)
TIME TO PEAK     (hrs)=          1.29          1.58          1.292
RUNOFF VOLUME    (mm)=          30.95          9.22          14.107
TOTAL RAINFALL   (mm)=          32.95          32.95          32.954
RUNOFF COEFFICIENT =          .94          .28          .428

                                *TOTALS*

```

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 81.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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002:0005-----
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*      TRIBUTARY AREAS TO SWM POND

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-----
| CALIB NASHYD      | Area    (ha)=    1.13    Curve Number  (CN)=75.00
| 03:203    DT= 2.00 | Ia      (mm)=    5.000    # of Linear Res.(N)= 3.00
-----
                        U.H. Tp(hrs)=    .180

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Unit Hyd Qpeak  (cms)=    .240

PEAK FLOW        (cms)=    .029 (i)
TIME TO PEAK     (hrs)=    1.500
RUNOFF VOLUME    (mm)=    6.938
TOTAL RAINFALL   (mm)=    32.954
RUNOFF COEFFICIENT =    .211

```

- (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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002:0006-----							

ADD HYD (	9)	ID: NHYD	AREA	QPEAK	TPEAK	R.V.	DWF
(cms)			(ha)	(cms)	(hrs)	(mm)	
	ID1 01:201		13.62	1.479	1.29	21.66	
.000							
	+ID2 02:202		2.58	.120	1.29	14.11	
.000							
	+ID3 03:203		1.13	.029	1.50	6.94	
.000							
=====							
	SUM 04:	9	17.33	1.610	1.29	19.57	
.000							

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

002:0007-----

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*ROUTE RUNOFF THROUGH PROPOSED POND

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ROUTE RESERVOIR		Requested routing time step = 2.0 min.			
IN>04:(000009)					
OUT<05:(000204)		===== OUTFLOW STORAGE TABLE =====			
-----		OUTFLOW	STORAGE	OUTFLOW	STORAGE
		(cms)	(ha.m.)	(cms)	(ha.m.)
		.000	.0000E+00	.026	.1010E+01
		.026	.3121E-01	.000	.0000E+00

ROUTING RESULTS	AREA	QPEAK	TPEAK	R.V.
-----	(ha)	(cms)	(hrs)	(mm)
INFLOW >04: (000009)	17.33	1.610	1.292	19.573
OUTFLOW<05: (000204)	17.33	.026	1.208	19.573
OVERFLOW<06: (000205)	.00	.000	.000	.000

TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
 CUMULATIVE TIME OF OVERFLOWS (hours)= .00
 PERCENTAGE OF TIME OVERFLOWING (%)= .00

PEAK FLOW REDUCTION [Qout/Qin](%)= 1.615
 TIME SHIFT OF PEAK FLOW (min)= -5.00
 MAXIMUM STORAGE USED (ha.m.)=.3152E+00


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002:0008-----
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002:0002-----
-----
** END OF RUN :    4

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-----
| START          | Project dir.: Q:\55926\100\202505~1\SWMHYMO\
----- Rainfall dir.: Q:\55926\100\202505~1\SWMHYMO\

    TZERO =    .00 hrs on          0
    METOUT=    2 (output = METRIC)
    NRUN   = 005
    NSTORM=    1
           #   1=5YR.HYT
-----
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005:0002-----
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*******
**
**# Project Name: [GLENDON ROAD]    Project Number: [55926-100]

**# Date           : OCTOBER 2024

**# Modeller       : [JJM]

**# Company        : MTE CONSULTANTS INC.

**# License #      :

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005:0002-----
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| READ STORM      | Filename: 5YR Chicago 3-hr duration

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| Ptotal= 44.47 mm| Comments: 5YR Chicago 3-hr duration

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	2.889	.92	10.155	1.75	11.292	2.58	3.967
.17	3.102	1.00	13.656	1.83	9.520	2.67	3.731
.25	3.352	1.08	20.548	1.92	8.224	2.75	3.523
.33	3.649	1.17	38.765	2.00	7.239	2.83	3.338
.42	4.007	1.25	141.200	2.08	6.466	2.92	3.173
.50	4.447	1.33	76.415	2.17	5.844	3.00	3.024
.58	5.002	1.42	38.412	2.25	5.333	3.08	2.889
.67	5.722	1.50	24.610	2.33	4.907		
.75	6.693	1.58	17.806	2.42	4.545		
.83	8.068	1.67	13.848	2.50	4.235		

005:0003

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* TRIBUTARY AREAS TO THE SOUTH OF STREET C

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CALIB STANDHYD	Area	(ha)=	13.62		
01:201 DT= 2.00	Total Imp(%)=	62.00	Dir. Conn.(%)=	56.00	

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	8.44	5.18	
Dep. Storage (mm)=	2.00	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	520.00	25.00	
Mannings n =	.015	.250	
Max.eff.Inten.(mm/hr)=	141.20	43.39	
over (min)	5.00	12.50	
Storage Coeff. (min)=	5.30 (ii)	12.73 (ii)	
Unit Hyd. Tpeak (min)=	5.00	12.50	
Unit Hyd. peak (cms)=	.22	.09	
			TOTALS
PEAK FLOW (cms)=	2.01	.37	2.149 (iii)
TIME TO PEAK (hrs)=	1.29	1.50	1.292
RUNOFF VOLUME (mm)=	42.47	16.97	31.248
TOTAL RAINFALL (mm)=	44.47	44.47	44.466
RUNOFF COEFFICIENT =	.96	.38	.703

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 80.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0004

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* TRIBUTARY AREAS TO THE NORTH OF STREET C

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CALIB STANDHYD	Area (ha)=	2.58		
02:202 DT= 2.00	Total Imp(%)=	25.00	Dir. Conn.(%)=	22.50

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	.64	1.93
Dep. Storage (mm)=	2.00	5.00
Average Slope (%)=	.80	2.00
Length (m)=	331.00	25.00
Mannings n =	.015	.250

Max.eff.Inten.(mm/hr)=	141.20	36.59
over (min)	5.00	12.50
Storage Coeff. (min)=	5.32 (ii)	13.28 (ii)
Unit Hyd. Tpeak (min)=	5.00	12.50
Unit Hyd. peak (cms)=	.21	.09

			TOTALS
PEAK FLOW (cms)=	.15	.11	.214 (iii)
TIME TO PEAK (hrs)=	1.29	1.50	1.375
RUNOFF VOLUME (mm)=	42.47	16.14	22.065
TOTAL RAINFALL (mm)=	44.47	44.47	44.466
RUNOFF COEFFICIENT =	.96	.36	.496

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 81.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0005

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* TRIBUTARY AREAS TO SWM POND

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CALIB NASHYD	Area (ha)=	1.13	Curve Number (CN)=	75.00
03:203 DT= 2.00	Ia (mm)=	5.000	# of Linear Res.(N)=	3.00

----- U.H. Tp(hrs)= .180

Unit Hyd Qpeak (cms)= .240

PEAK FLOW (cms)= .054 (i)

TIME TO PEAK (hrs)= 1.500

RUNOFF VOLUME (mm)= 12.548

TOTAL RAINFALL (mm)= 44.466

RUNOFF COEFFICIENT = .282

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0006-----

ADD HYD (	9) ID: NHYD	AREA	QPEAK	TPEAK	R.V.	DWF
(cms)		(ha)	(cms)	(hrs)	(mm)	
	ID1 01:201	13.62	2.149	1.29	31.25	
.000						
	+ID2 02:202	2.58	.214	1.38	22.06	
.000						
	+ID3 03:203	1.13	.054	1.50	12.55	
.000						
=====						
	SUM 04:	9	17.33	2.369	1.29	28.66
.000						

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

005:0007-----

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*ROUTE RUNOFF THROUGH PROPOSED POND

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ROUTE RESERVOIR		Requested routing time step = 2.0 min.
IN>04:(000009)		
OUT<05:(000204)		
=====		
OUTFLOW STORAGE TABLE		
OUTFLOW	STORAGE	OUTFLOW STORAGE
(cms)	(ha.m.)	(cms) (ha.m.)
.000	.0000E+00	.026 .1010E+01
.026	.3121E-01	.000 .0000E+00

ROUTING RESULTS

AREA

QPEAK

TPEAK

R.V.

	(ha)	(cms)	(hrs)	(mm)
INFLOW >04: (000009)	17.33	2.369	1.292	28.661
OUTFLOW<05: (000204)	17.33	.026	1.125	28.661
OVERFLOW<06: (000205)	.00	.000	.000	.000

TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
 CUMULATIVE TIME OF OVERFLOWS (hours)= .00
 PERCENTAGE OF TIME OVERFLOWING (%)= .00

PEAK FLOW REDUCTION [Qout/Qin](%)= 1.098
 TIME SHIFT OF PEAK FLOW (min)= -10.00
 MAXIMUM STORAGE USED (ha.m.)=.4720E+00

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005:0008-----
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005:0002-----
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005:0002-----
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** END OF RUN : 9
  
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| START          | Project dir.: Q:\55926\100\202505~1\SWMHYMO\
----- Rainfall dir.: Q:\55926\100\202505~1\SWMHYMO\

TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 010
NSTORM= 1
# 1=10YR.HYT
  
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010:0002-----
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*#####
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*# Project Name: [GLENDON ROAD] Project Number: [55926-100]

*# Date : OCTOBER 2024

*# Modeller : [JJM]

*# Company : MTE CONSULTANTS INC.

*# License # :

*#*****
**

010:0002

| READ STORM | Filename: 10YR Chicago 3-hr duration
| Ptotal= 52.37 mm | Comments: 10YR Chicago 3-hr duration

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	3.141	.92	11.986	1.75	13.417	2.58	4.407
.17	3.389	1.00	16.365	1.83	11.203	2.67	4.128
.25	3.681	1.08	25.006	1.92	9.593	2.75	3.882
.33	4.030	1.17	47.536	2.00	8.375	2.83	3.665
.42	4.454	1.25	162.500	2.08	7.426	2.92	3.472
.50	4.979	1.33	92.425	2.17	6.667	3.00	3.298
.58	5.645	1.42	47.240	2.25	6.047	3.08	3.141
.67	6.517	1.50	30.137	2.33	5.531		
.75	7.701	1.58	21.600	2.42	5.097		
.83	9.394	1.67	16.623	2.50	4.727		

010:0003

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* TRIBUTARY AREAS TO THE SOUTH OF STREET C

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| CALIB STANDHYD | Area (ha)= 13.62
| 01:201 DT= 2.00 | Total Imp(%)= 62.00 Dir. Conn.(%)= 56.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	8.44	5.18
Dep. Storage	(mm)=	2.00	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	520.00	25.00
Mannings n	=	.015	.250

Max.eff.Inten.(mm/hr)=	162.50	58.24	
over (min)	5.00	12.50	
Storage Coeff. (min)=	5.01 (ii)	11.62 (ii)	
Unit Hyd. Tpeak (min)=	5.00	12.50	
Unit Hyd. peak (cms)=	.22	.09	
			TOTALS
PEAK FLOW (cms)=	2.39	.52	2.599 (iii)
TIME TO PEAK (hrs)=	1.29	1.46	1.292
RUNOFF VOLUME (mm)=	50.37	22.44	38.080
TOTAL RAINFALL (mm)=	52.37	52.37	52.369
RUNOFF COEFFICIENT =	.96	.43	.727

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 80.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0004-

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* TRIBUTARY AREAS TO THE NORTH OF STREET C

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CALIB STANDHYD	Area (ha)=	2.58	
02:202 DT= 2.00	Total Imp(%)=	25.00	Dir. Conn.(%)= 22.50

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	.64	1.93	
Dep. Storage (mm)=	2.00	5.00	
Average Slope (%)=	.80	2.00	
Length (m)=	331.00	25.00	
Mannings n =	.015	.250	
Max.eff.Inten.(mm/hr)=	162.50	49.50	
over (min)	5.00	12.50	
Storage Coeff. (min)=	5.03 (ii)	12.08 (ii)	
Unit Hyd. Tpeak (min)=	5.00	12.50	
Unit Hyd. peak (cms)=	.22	.09	
			TOTALS
PEAK FLOW (cms)=	.18	.16	.279 (iii)
TIME TO PEAK (hrs)=	1.29	1.50	1.375
RUNOFF VOLUME (mm)=	50.37	21.48	27.978
TOTAL RAINFALL (mm)=	52.37	52.37	52.369
RUNOFF COEFFICIENT =	.96	.41	.534

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:

- CN* = 81.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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010:0005-----
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*      TRIBUTARY AREAS TO SWM POND
*=====
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-----
| CALIB NASHYD      | Area   (ha)=   1.13   Curve Number (CN)=75.00
| 03:203   DT= 2.00 | Ia     (mm)=  5.000   # of Linear Res.(N)= 3.00
-----
                        U.H. Tp(hrs)=   .180

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Unit Hyd Qpeak (cms)= .240

PEAK FLOW (cms)= .076 (i)

TIME TO PEAK (hrs)= 1.500

RUNOFF VOLUME (mm)= 16.994

TOTAL RAINFALL (mm)= 52.369

RUNOFF COEFFICIENT = .325

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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010:0006-----
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| ADD HYD (          9) | ID: NHYD      AREA   QPEAK  TPEAK  R.V.   DWF
-----
(cms)                                (ha)   (cms)   (hrs)   (mm)
                        ID1 01:201      13.62   2.599   1.29   38.08
.000
                        +ID2 02:202       2.58   .279    1.38   27.98
.000
                        +ID3 03:203       1.13   .076    1.50   16.99
.000
=====
                        SUM 04:          9   17.33   2.880   1.29   35.20
.000

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NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.


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010:0007-----
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*ROUTE RUNOFF THROUGH PROPOSED POND
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| ROUTE RESERVOIR | Requested routing time step = 2.0 min.
| IN>04:(000009) |
| OUT<05:(000204) |
-----
===== OUTFLOW STORAGE TABLE =====
OUTFLOW    STORAGE | OUTFLOW    STORAGE
  (cms)      (ha.m.) |   (cms)      (ha.m.)
    .000    .0000E+00 |    .026    .1010E+01
    .026    .3121E-01 |    .000    .0000E+00

ROUTING RESULTS          AREA      QPEAK      TPEAK      R.V.
-----
INFLOW >04: (000009)    17.33      2.880      1.292     35.201
OUTFLOW<05: (000204)    17.33      .026      1.083     35.201
OVERFLOW<06: (000205)     .00      .000      .000      .000

TOTAL NUMBER OF SIMULATED OVERFLOWS =          0
CUMULATIVE TIME OF OVERFLOWS (hours)=          .00
PERCENTAGE OF TIME OVERFLOWING (%)=          .00

PEAK FLOW REDUCTION [Qout/Qin](%)=          .903
TIME SHIFT OF PEAK FLOW (min)=        -12.50
MAXIMUM STORAGE USED (ha.m.)=.5849E+00

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010:0008-----
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010:0002-----
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010:0002-----
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010:0002-----
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010:0002-----
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** END OF RUN : 24

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| START          | Project dir.: Q:\55926\100\202505~1\SWMHYMO\
----- Rainfall dir.: Q:\55926\100\202505~1\SWMHYMO\

TZERO = .00 hrs on      0
METOUT= 2 (output = METRIC)
NRUN   = 025
NSTORM= 1
      # 1=25YR.HYT
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025:0002-----
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**#*****
**
*# Project Name: [GLENDON ROAD]    Project Number: [55926-100]

*# Date           : OCTOBER 2024

*# Modeller       : [JJM]

*# Company        : MTE CONSULTANTS INC.

*# License #      :

**#*****
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025:0002-----
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-----
| READ STORM      | Filename: 25YR Chicago 3-hr duration
| Ptotal= 61.85 mm| Comments: 25YR Chicago 3-hr duration
-----

      TIME    RAIN |    TIME    RAIN |    TIME    RAIN |    TIME    RAIN
      hrs     mm/hr |    hrs     mm/hr |    hrs     mm/hr |    hrs     mm/hr
      .08    3.490 |    .92   14.107 |    1.75   15.861 |    2.58    4.972
      .17    3.779 |    1.00   19.457 |    1.83   13.158 |    2.67    4.644
      .25    4.120 |    1.08   30.035 |    1.92   11.200 |    2.75    4.356
      .33    4.529 |    1.17   57.437 |    2.00    9.725 |    2.83    4.101
      .42    5.028 |    1.25  190.801 |    2.08    8.578 |    2.92    3.875
      .50    5.649 |    1.33  111.064 |    2.17    7.665 |    3.00    3.672
      .58    6.442 |    1.42   57.174 |    2.25    6.922 |    3.08    3.490
      .67    7.484 |    1.50   36.348 |    2.33    6.307 |
      .75    8.908 |    1.58   25.889 |    2.42    5.790 |
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.83 10.956 | 1.67 19.786 | 2.50 5.351 |

025:0003

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TRIBUTARY AREAS TO THE SOUTH OF STREET C

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CALIB STANDHYD	Area (ha)=	13.62
01:201 DT= 2.00	Total Imp(%)=	62.00 Dir. Conn.(%)= 56.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	8.44	5.18
Dep. Storage	(mm)=	2.00	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	520.00	25.00
Mannings n	=	.015	.250

Max.eff.Inten.(mm/hr)=	190.80	86.57
over (min)	5.00	10.00
Storage Coeff. (min)=	4.70 (ii)	10.34 (ii)
Unit Hyd. Tpeak (min)=	5.00	10.00
Unit Hyd. peak (cms)=	.23	.11

			TOTALS
PEAK FLOW	(cms)=	2.88	.75 3.285 (iii)
TIME TO PEAK	(hrs)=	1.29	1.42 1.292
RUNOFF VOLUME	(mm)=	59.85	29.45 46.472
TOTAL RAINFALL	(mm)=	61.85	61.85 61.846
RUNOFF COEFFICIENT	=	.97	.48 .751

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:

CN* = 80.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0004

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TRIBUTARY AREAS TO THE NORTH OF STREET C

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CALIB STANDHYD	Area (ha)=	2.58
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| 02:202 DT= 2.00 | Total Imp(%)= 25.00 Dir. Conn.(%)= 22.50

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	.64	1.93	
Dep. Storage	(mm)=	2.00	5.00	
Average Slope	(%)=	.80	2.00	
Length	(m)=	331.00	25.00	
Mannings n	=	.015	.250	
Max.eff.Inten.(mm/hr)=		190.80	73.98	
over (min)		5.00	10.00	
Storage Coeff. (min)=		4.71 (ii)	10.72 (ii)	
Unit Hyd. Tpeak (min)=		5.00	10.00	
Unit Hyd. peak (cms)=		.23	.11	
				TOTALS
PEAK FLOW	(cms)=	.22	.24	.399 (iii)
TIME TO PEAK	(hrs)=	1.29	1.46	1.375
RUNOFF VOLUME	(mm)=	59.85	28.34	35.430
TOTAL RAINFALL	(mm)=	61.85	61.85	61.846
RUNOFF COEFFICIENT	=	.97	.46	.573

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 81.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0005-

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* TRIBUTARY AREAS TO SWM POND

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CALIB NASHYD		Area	(ha)=	1.13	Curve Number (CN)=75.00
03:203 DT= 2.00		Ia	(mm)=	5.000	# of Linear Res.(N)= 3.00
-----		U.H. Tp(hrs)=		.180	

Unit Hyd Qpeak (cms)= .240

PEAK FLOW (cms)= .104 (i)

TIME TO PEAK (hrs)= 1.458

RUNOFF VOLUME (mm)= 22.835

TOTAL RAINFALL (mm)= 61.846

RUNOFF COEFFICIENT = .369

- (i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0006-----

ADD HYD (9) ID: NHYD		AREA	QPEAK	TPEAK	R.V.	DWF
		(ha)	(cms)	(hrs)	(mm)	
(cms)						
	ID1 01:201	13.62	3.285	1.29	46.47	
.000						
	+ID2 02:202	2.58	.399	1.38	35.43	
.000						
	+ID3 03:203	1.13	.104	1.46	22.83	
.000						
=====						
	SUM 04:	9	17.33	3.705	1.33	43.29
.000						

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

025:0007-----

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*ROUTE RUNOFF THROUGH PROPOSED POND

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ROUTE RESERVOIR		Requested routing time step = 2.0 min.			
IN>04:(000009)					
OUT<05:(000204)		===== OUTFLOW STORAGE TABLE =====			
		OUTFLOW	STORAGE	OUTFLOW	STORAGE
		(cms)	(ha.m.)	(cms)	(ha.m.)
		.000	.0000E+00	.026	.1010E+01
		.026	.3121E-01	.000	.0000E+00

ROUTING RESULTS	AREA	QPEAK	TPEAK	R.V.
-----	(ha)	(cms)	(hrs)	(mm)
INFLOW >04: (000009)	17.33	3.705	1.333	43.287
OUTFLOW<05: (000204)	17.33	.026	1.000	43.287
OVERFLOW<06: (000205)	.00	.000	.000	.000

TOTAL NUMBER OF SIMULATED OVERFLOWS = 0

CUMULATIVE TIME OF OVERFLOWS (hours)= .00

PERCENTAGE OF TIME OVERFLOWING (%)= .00

PEAK FLOW REDUCTION [Qout/Qin](%)= .702

TIME SHIFT OF PEAK FLOW (min)= -20.00

MAXIMUM STORAGE USED (ha.m.)=.7248E+00

025:0008-----

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025:0002-----

025:0002-----

025:0002-----

025:0002-----

025:0002-----

025:0002-----

** END OF RUN : 49

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| START | Project dir.: Q:\55926\100\202505~1\SWMHYMO\
----- Rainfall dir.: Q:\55926\100\202505~1\SWMHYMO\

TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 050
NSTORM= 1
1=50YR.HYT

050:0002-----

*#*****
**
*# Project Name: [GLENDON ROAD] Project Number: [55926-100]
*# Date : OCTOBER 2024
*# Modeller : [JJM]

*# Company : MTE CONSULTANTS INC.

*# License # :

*#*****
**

050:0002-----

| READ STORM | Filename: 50YR Chicago 3-hr duration
| Ptotal= 69.13 mm | Comments: 50YR Chicago 3-hr duration

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	3.895	.92	15.824	1.75	17.797	2.58	5.558
.17	4.219	1.00	21.837	1.83	14.758	2.67	5.189
.25	4.601	1.08	33.713	1.92	12.556	2.75	4.866
.33	5.060	1.17	64.387	2.00	10.897	2.83	4.580
.42	5.620	1.25	212.001	2.08	9.609	2.92	4.326
.50	6.318	1.33	124.085	2.17	8.582	3.00	4.100
.58	7.208	1.42	64.104	2.25	7.747	3.08	3.895
.67	8.379	1.50	40.797	2.33	7.057		
.75	9.980	1.58	29.062	2.42	6.476		
.83	12.281	1.67	22.208	2.50	5.983		

050:0003-----

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* TRIBUTARY AREAS TO THE SOUTH OF STREET C

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| CALIB STANDHYD | Area (ha)= 13.62
| 01:201 DT= 2.00 | Total Imp(%)= 62.00 Dir. Conn.(%)= 56.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	8.44	5.18
Dep. Storage (mm)=	2.00	5.00
Average Slope (%)=	2.00	2.00
Length (m)=	520.00	25.00
Mannings n =	.015	.250
Max.eff.Inten.(mm/hr)=	212.00	103.72
over (min)	5.00	10.00
Storage Coeff. (min)=	4.50 (ii)	9.75 (ii)
Unit Hyd. Tpeak (min)=	5.00	10.00

Unit Hyd. peak (cms)=	.24	.11	
			TOTALS
PEAK FLOW (cms)=	3.25	.93	3.764 (iii)
TIME TO PEAK (hrs)=	1.29	1.42	1.292
RUNOFF VOLUME (mm)=	67.13	35.11	53.039
TOTAL RAINFALL (mm)=	69.13	69.13	69.130
RUNOFF COEFFICIENT =	.97	.51	.767

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 80.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 050:0004-----

 *=====

=
 * TRIBUTARY AREAS TO THE NORTH OF STREET C

*=====

CALIB STANDHYD	Area (ha)=	2.58	
02:202 DT= 2.00	Total Imp(%)=	25.00	Dir. Conn.(%)= 22.50

		IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	.64		1.93
Dep. Storage (mm)=	2.00		5.00
Average Slope (%)=	.80		2.00
Length (m)=	331.00		25.00
Mannings n =	.015		.250
Max.eff.Inten.(mm/hr)=	212.00		89.01
over (min)	5.00		10.00
Storage Coeff. (min)=	4.52 (ii)		10.10 (ii)
Unit Hyd. Tpeak (min)=	5.00		10.00
Unit Hyd. peak (cms)=	.24		.11
			TOTALS
PEAK FLOW (cms)=	.25	.29	.476 (iii)
TIME TO PEAK (hrs)=	1.29	1.42	1.375
RUNOFF VOLUME (mm)=	67.13	33.89	41.372
TOTAL RAINFALL (mm)=	69.13	69.13	69.130
RUNOFF COEFFICIENT =	.97	.49	.598

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 81.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

050:0005-----

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* TRIBUTARY AREAS TO SWM POND

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| CALIB NASHYD | Area (ha)= 1.13 Curve Number (CN)=75.00
| 03:203 DT= 2.00 | Ia (mm)= 5.000 # of Linear Res.(N)= 3.00

 U.H. Tp(hrs)= .180

Unit Hyd Qpeak (cms)= .240

PEAK FLOW (cms)= .127 (i)

TIME TO PEAK (hrs)= 1.458

RUNOFF VOLUME (mm)= 27.639

TOTAL RAINFALL (mm)= 69.130

RUNOFF COEFFICIENT = .400

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

050:0006-----

| ADD HYD (9) | ID: NHYD AREA QPEAK TPEAK R.V. DWF

 (ha) (cms) (hrs) (mm)
(cms)
 ID1 01:201 13.62 3.764 1.29 53.04
.000
 +ID2 02:202 2.58 .476 1.38 41.37
.000
 +ID3 03:203 1.13 .127 1.46 27.64
.000

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	SUM 04:	9	17.33	4.270	1.33	49.65
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.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

050:0007-----

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*ROUTE RUNOFF THROUGH PROPOSED POND

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050:0008-----
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050:0002-----
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050:0002-----
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050:0002-----
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050:0002-----
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050:0002-----
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** END OF RUN : 99

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| START | Project dir.: Q:\55926\100\202505~1\SWMHYMO\

----- Rainfall dir.: Q:\55926\100\202505~1\SWMHYMO\

TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 100
NSTORM= 1
1=100YR.HYT

100:0002-----

*#*****
**

*# Project Name: [GLENDON ROAD] Project Number: [55926-100]

*# Date : OCTOBER 2024

*# Modeller : [JJM]

*# Company : MTE CONSULTANTS INC.

*# License # :

*#*****
**

100:0002-----

| READ STORM | Filename: 100YR Chicago 3-hr duration
| Ptotal= 76.27 mm | Comments: 100YR Chicago 3-hr duration

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	4.164	.92	17.483	1.75	19.709	2.58	5.997
.17	4.519	1.00	24.251	1.83	16.288	2.67	5.589
.25	4.940	1.08	37.617	1.92	13.813	2.75	5.232
.33	5.447	1.17	71.935	2.00	11.952	2.83	4.917
.42	6.066	1.25	232.200	2.08	10.509	2.92	4.638
.50	6.839	1.33	137.906	2.17	9.361	3.00	4.388

.58	7.828		1.42	71.694		2.25	8.430		3.08	4.164
.67	9.133		1.50	45.604		2.33	7.661			
.75	10.922		1.58	32.403		2.42	7.015			
.83	13.502		1.67	24.679		2.50	6.467			

 100:0003-----

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* TRIBUTARY AREAS TO THE SOUTH OF STREET C

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CALIB STANDHYD		Area	(ha)=	13.62						
01:201 DT= 2.00		Total Imp(%)=	62.00	Dir. Conn.(%)=	56.00					

		IMPERVIOUS	PERVIOUS (i)	
Surface Area	(ha)=	8.44	5.18	
Dep. Storage	(mm)=	2.00	5.00	
Average Slope	(%)=	2.00	2.00	
Length	(m)=	520.00	25.00	
Mannings n	=	.015	.250	
Max.eff.Inten.(mm/hr)=		232.20	121.28	
over (min)		5.00	10.00	
Storage Coeff. (min)=		4.34 (ii)	9.27 (ii)	
Unit Hyd. Tpeak (min)=		5.00	10.00	
Unit Hyd. peak (cms)=		.24	.12	
				TOTALS
PEAK FLOW	(cms)=	3.61	1.11	4.245 (iii)
TIME TO PEAK	(hrs)=	1.29	1.42	1.292
RUNOFF VOLUME	(mm)=	74.27	40.83	59.559
TOTAL RAINFALL	(mm)=	76.27	76.27	76.272
RUNOFF COEFFICIENT	=	.97	.54	.781

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 80.0 Ia = Dep. Storage (Above)
 (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
 (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 100:0004-----

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* TRIBUTARY AREAS TO THE NORTH OF STREET C

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-----
| CALIB STANDHYD      | Area    (ha)=    2.58
| 02:202    DT= 2.00 | Total Imp(%)=   25.00  Dir. Conn.(%)=   22.50
-----
```

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	.64	1.93	
Dep. Storage (mm)=	2.00	5.00	
Average Slope (%)=	.80	2.00	
Length (m)=	331.00	25.00	
Mannings n =	.015	.250	
Max.eff.Inten.(mm/hr)=	232.20	104.43	
over (min)	5.00	10.00	
Storage Coeff. (min)=	4.36 (ii)	9.59 (ii)	
Unit Hyd. Tpeak (min)=	5.00	10.00	
Unit Hyd. peak (cms)=	.24	.12	
			TOTALS
PEAK FLOW (cms)=	.27	.35	.556 (iii)
TIME TO PEAK (hrs)=	1.29	1.42	1.375
RUNOFF VOLUME (mm)=	74.27	39.53	47.345
TOTAL RAINFALL (mm)=	76.27	76.27	76.272
RUNOFF COEFFICIENT =	.97	.52	.621

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 81.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0005-----

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* TRIBUTARY AREAS TO SWM POND

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-----
| CALIB NASHYD        | Area    (ha)=    1.13  Curve Number (CN)=75.00
| 03:203    DT= 2.00 | Ia      (mm)=    5.000  # of Linear Res.(N)= 3.00
-----
|                      | U.H. Tp(hrs)=    .180
```

Unit Hyd Qpeak (cms)=	.240
PEAK FLOW (cms)=	.151 (i)
TIME TO PEAK (hrs)=	1.458
RUNOFF VOLUME (mm)=	32.575
TOTAL RAINFALL (mm)=	76.272
RUNOFF COEFFICIENT =	.427

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0006-----							

ADD HYD (	9)	ID: NHYD	AREA	QPEAK	TPEAK	R.V.	DWF
(cms)			(ha)	(cms)	(hrs)	(mm)	
		ID1 01:201	13.62	4.245	1.29	59.56	
.000		+ID2 02:202	2.58	.556	1.38	47.35	
.000		+ID3 03:203	1.13	.151	1.46	32.57	
.000							
=====							
		SUM 04:	9	17.33	4.850	1.33	55.98
.000							

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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100:0007-----
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*ROUTE RUNOFF THROUGH PROPOSED POND
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| ROUTE RESERVOIR | Requested routing time step = 2.0 min.
| IN>04:(000009) |
| OUT<05:(000204) |
-----
===== OUTFLOW STORAGE TABLE =====
OUTFLOW    STORAGE    |    OUTFLOW    STORAGE
   (cms)    (ha.m.)    |    (cms)    (ha.m.)
     .000    .0000E+00    |     .026    .1010E+01
     .026    .3121E-01    |     .000    .0000E+00

ROUTING RESULTS          AREA      QPEAK      TPEAK      R.V.
-----
                        (ha)      (cms)      (hrs)      (mm)
INFLOW >04: (000009)    17.33     4.850     1.333     55.981
OUTFLOW<05: (000204)    17.33      .026      .917     55.981
OVERFLOW<06: (000205)   .00      .000      .000      .000

TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
CUMULATIVE TIME OF OVERFLOWS (hours)= .00
PERCENTAGE OF TIME OVERFLOWING (%)= .00

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100:0008-----
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100:0002-----
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100:0002-----
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100:0002-----
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FINISH
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*****
*****
WARNINGS / ERRORS / NOTES
-----
Simulation ended on 2025-05-27      at 13:13:25
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===
SSSSS W W M M H H Y Y M M 000 999 999
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S W W W MM MM H H Y Y MM MM O O 9 9 9 9
SSSSS W W W M M M HHHHH Y M M M O O ## 9 9 9 9 Ver
4.05
S W W M M H H Y M M O O 9999 9999 Sept
2011
SSSSS W W M M H H Y M M 000 9 9
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9 9 9 9 #
3053466
StormWater Management HYdrologic Model 999 999
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*****
*
***** SWMHYMO Ver/4.05
*****
***** A single event and continuous hydrologic simulation model
*****
***** based on the principles of HYMO and its successors
*****
***** OTTHYMO-83 and OTTHYMO-89.
*****

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*****
*
***** Distributed by: J.F. Sabourin and Associates Inc.
*****
***** Ottawa, Ontario: (613) 836-3884
*****
***** Gatineau, Quebec: (819) 243-6858
*****
***** E-Mail: swmhymo@jfsa.Com
*****

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*****
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+++++
+
+++++ Licensed user: MTE Consultants Inc.
+++++
+++++ Burlington SERIAL#:3053466
+++++
+++++
+

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*****
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* *****
*          ++++++ PROGRAM ARRAY DIMENSIONS ++++++
* *****
* *****
*          Maximum value for ID numbers   :    10
* *****
* *****
*          Max. number of rainfall points: 105408
* *****
* *****
*          Max. number of flow points     : 105408
* *****
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*****
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*****      D E T A I L E D   O U T P U T
*****
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*****
*
*          DATE: 2025-05-27      TIME: 13:53:47      RUN COUNTER: 000034
*
```

```
*****
*
* Input   filename: Q:\55926\100\202505~1\SWMHYMO\POST_UCN.DAT
*
* Output  filename: Q:\55926\100\202505~1\SWMHYMO\POST_UCN.out
*
* Summary filename: Q:\55926\100\202505~1\SWMHYMO\POST_UCN.sum
*
* User comments:
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1: _____*
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2: _____*
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3: _____*
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001:0001-----
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*#*****
**
*# Project Name: [GLENDON ROAD]      Project Number: [55926-100]
```

*# Date : OCTOBER 2024
*# Modeller : [JJM]
*# Company : MTE CONSULTANTS INC.
*# License # :

**

| START | Project dir.: Q:\55926\100\202505~1\SWMHYMO\

----- Rainfall dir.: Q:\55926\100\202505~1\SWMHYMO\

TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 001
NSTORM= 1
1=25mm.HYT

001:0002-----

| READ STORM | Filename: 25mm Chicago 4-hr duration
| Ptotal= 24.83 mm | Comments: 25mm Chicago 4-hr duration

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	1.326	1.17	3.978	2.25	4.889	3.33	1.844
.17	1.392	1.25	4.803	2.33	4.304	3.42	1.765
.25	1.466	1.33	6.089	2.42	3.849	3.50	1.693
.33	1.549	1.42	8.350	2.50	3.485	3.58	1.627
.42	1.643	1.50	13.259	2.58	3.187	3.67	1.567
.50	1.750	1.58	29.925	2.67	2.939	3.75	1.511
.58	1.875	1.67	75.600	2.75	2.729	3.83	1.460
.67	2.020	1.75	27.475	2.83	2.549	3.92	1.412
.75	2.193	1.83	15.856	2.92	2.392	4.00	1.368
.83	2.401	1.92	10.977	3.00	2.256	4.08	1.326
.92	2.657	2.00	8.363	3.08	2.135		
1.00	2.981	2.08	6.752	3.17	2.027		
1.08	3.404	2.17	5.667	3.25	1.930		

001:0003-----

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* TRIBUTARY AREAS TO STREET A SOUTH TO GLENDON DRIVE (UNCONTROLLED)

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-----
| CALIB STANDHYD      | Area   (ha)=   1.13
| 06:301    DT= 2.00 | Total Imp(%)= 45.00  Dir. Conn.(%)= 40.00
-----
```

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	.51	.62
Dep. Storage	(mm)=	2.00	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	57.00	5.50
Mannings n	=	.015	.250

Max.eff.Inten.(mm/hr)=	75.60	45.52
over (min)	2.50	5.00
Storage Coeff. (min)=	1.80 (ii)	4.74 (ii)
Unit Hyd. Tpeak (min)=	2.50	5.00
Unit Hyd. peak (cms)=	.51	.23

TOTALS

PEAK FLOW	(cms)=	.09	.05	.134 (iii)
TIME TO PEAK	(hrs)=	1.67	1.71	1.667
RUNOFF VOLUME	(mm)=	22.83	12.62	16.702
TOTAL RAINFALL	(mm)=	24.83	24.83	24.833
RUNOFF COEFFICIENT	=	.92	.51	.673

*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 95.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0004-----

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* TRIBUTARY AREAS TO ADJACENT PROPERTY TO THE WEST (UNCONTROLLED)

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-----
| CALIB STANDHYD      | Area   (ha)=   1.13
| 07:302    DT= 2.00 | Total Imp(%)= 45.00  Dir. Conn.(%)= 40.00
-----
```

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	.51	.62
Dep. Storage	(mm)=	2.00	5.00
Average Slope	(%)=	1.80	2.00
Length	(m)=	105.00	5.50
Mannings n	=	.015	.250

*** NOTE: User defined Storage Coefficients were used
for Unit Hydrograph calculations.

Max.eff.Inten.(mm/hr)=	75.60	45.52	
over (min)	2.50	5.00	
Storage Coeff. (min)=	2.00 (ii)	4.94 (ii)	
Unit Hyd. Tpeak (min)=	2.50	5.00	
Unit Hyd. peak (cms)=	.48	.23	
			TOTALS
PEAK FLOW (cms)=	.09	.05	.132 (iii)
TIME TO PEAK (hrs)=	1.67	1.71	1.667
RUNOFF VOLUME (mm)=	22.83	12.62	16.702
TOTAL RAINFALL (mm)=	24.83	24.83	24.833
RUNOFF COEFFICIENT =	.92	.51	.673

*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 95.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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001:0005-----
-----
| ADD HYD (      303) | ID: NHYD      AREA      QPEAK      TPEAK      R.V.      DWF
-----
(cms)
                ID1 06:301          1.13      .134      1.67      16.70
.000
                +ID2 07:302          1.13      .132      1.67      16.70
.000

=====
                SUM 08:      303      2.26      .267      1.67      16.70
.000

```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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001:0006-----
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** END OF RUN :    1

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| START | Project dir.: Q:\55926\100\202505~1\SWMHYMO\

----- Rainfall dir.: Q:\55926\100\202505~1\SWMHYMO\

TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 002
NSTORM= 1
1=2YR.HYT

002:0002-----

*#*****

**

*# Project Name: [GLENDON ROAD] Project Number: [55926-100]

*# Date : OCTOBER 2024

*# Modeller : [JJM]

*# Company : MTE CONSULTANTS INC.

*# License # :

*#*****

**

002:0002-----

| READ STORM | Filename: 2YR Chicago 3-hr duration
| Ptotal= 32.95 mm | Comments: 2YR Chicago 3-hr duration

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	2.366	.92	7.556	1.75	8.343	2.58	3.173
.17	2.528	1.00	9.957	1.83	7.120	2.67	2.999
.25	2.716	1.08	14.640	1.92	6.218	2.75	2.844
.33	2.938	1.17	27.128	2.00	5.527	2.83	2.706
.42	3.203	1.25	106.663	2.08	4.980	2.92	2.581
.50	3.527	1.33	54.508	2.17	4.537	3.00	2.469
.58	3.931	1.42	26.925	2.25	4.170	3.08	2.366
.67	4.449	1.50	17.418	2.33	3.862		
.75	5.140	1.58	12.788	2.42	3.599		
.83	6.108	1.67	10.093	2.50	3.372		

002:0003-----

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*=====
=
*      TRIBUTARY AREAS TO STREET A SOUTH TO GLENDON DRIVE (UNCONTROLLED)

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-----
| CALIB STANDHYD | Area (ha)= 1.13
| 06:301 DT= 2.00 | Total Imp(%)= 45.00 Dir. Conn.(%)= 40.00
-----

```

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	.51	.62
Dep. Storage	(mm)=	2.00	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	57.00	5.50
Mannings n	=	.015	.250

Max.eff.Inten.(mm/hr)=	106.66	71.03
over (min)	2.50	5.00
Storage Coeff. (min)=	1.57 (ii)	4.03 (ii)
Unit Hyd. Tpeak (min)=	2.50	5.00
Unit Hyd. peak (cms)=	.54	.26

TOTALS

PEAK FLOW	(cms)=	.13	.09	.201 (iii)
TIME TO PEAK	(hrs)=	1.25	1.29	1.250
RUNOFF VOLUME	(mm)=	30.95	19.81	24.269
TOTAL RAINFALL	(mm)=	32.95	32.95	32.954
RUNOFF COEFFICIENT	=	.94	.60	.736

*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 95.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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002:0004-----
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=
*      TRIBUTARY AREAS TO ADJACENT PROPERTY TO THE WEST (UNCONTROLLED)

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-----
| CALIB STANDHYD | Area (ha)= 1.13
| 07:302 DT= 2.00 | Total Imp(%)= 45.00 Dir. Conn.(%)= 40.00
-----

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		IMPERVIOUS	PERVIOUS (i)
--	--	------------	--------------

Surface Area	(ha)=	.51	.62
Dep. Storage	(mm)=	2.00	5.00
Average Slope	(%)=	1.80	2.00
Length	(m)=	105.00	5.50
Mannings n	=	.015	.250

*** NOTE: User defined Storage Coefficients were used
for Unit Hydrograph calculations.

Max.eff.Inten.(mm/hr)=	106.66	71.03
over (min)	2.50	5.00
Storage Coeff. (min)=	2.00 (ii)	4.46 (ii)
Unit Hyd. Tpeak (min)=	2.50	5.00
Unit Hyd. peak (cms)=	.48	.24

TOTALS

PEAK FLOW	(cms)=	.13	.09	.193 (iii)
TIME TO PEAK	(hrs)=	1.25	1.29	1.250
RUNOFF VOLUME	(mm)=	30.95	19.81	24.269
TOTAL RAINFALL	(mm)=	32.95	32.95	32.954
RUNOFF COEFFICIENT	=	.94	.60	.736

*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 95.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0005

ADD HYD (	303)	ID: NHYD	AREA	QPEAK	TPEAK	R.V.	DWF
(cms)			(ha)	(cms)	(hrs)	(mm)	
		ID1 06:301	1.13	.201	1.25	24.27	
.000		+ID2 07:302	1.13	.193	1.25	24.27	
.000							

	SUM 08:	303	2.26	.393	1.25	24.27
.000						

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

002:0006

002:0002-----

** END OF RUN : 4

*

| START | Project dir.: Q:\55926\100\202505~1\SWMHYMO\
----- Rainfall dir.: Q:\55926\100\202505~1\SWMHYMO\

TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 005
NSTORM= 1
1=5YR.HYT

005:0002-----

*#*****
**
*# Project Name: [GLENDON ROAD] Project Number: [55926-100]

*# Date : OCTOBER 2024

*# Modeller : [JJM]

*# Company : MTE CONSULTANTS INC.

*# License # :

*#*****
**

005:0002-----

| READ STORM | Filename: 5YR Chicago 3-hr duration
| Ptotal= 44.47 mm | Comments: 5YR Chicago 3-hr duration

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	2.889	.92	10.155	1.75	11.292	2.58	3.967
.17	3.102	1.00	13.656	1.83	9.520	2.67	3.731
.25	3.352	1.08	20.548	1.92	8.224	2.75	3.523
.33	3.649	1.17	38.765	2.00	7.239	2.83	3.338

.42	4.007		1.25	141.200		2.08	6.466		2.92	3.173
.50	4.447		1.33	76.415		2.17	5.844		3.00	3.024
.58	5.002		1.42	38.412		2.25	5.333		3.08	2.889
.67	5.722		1.50	24.610		2.33	4.907			
.75	6.693		1.58	17.806		2.42	4.545			
.83	8.068		1.67	13.848		2.50	4.235			

 005:0003-----

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* TRIBUTARY AREAS TO STREET A SOUTH TO GLENDON DRIVE (UNCONTROLLED)

*=====

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CALIB STANDHYD		Area (ha)=	1.13		
06:301 DT= 2.00		Total Imp(%)=	45.00	Dir. Conn.(%)=	40.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	.51	.62
Dep. Storage	(mm)=	2.00	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	57.00	5.50
Mannings n	=	.015	.250

Max.eff.Inten.(mm/hr)=	141.20	122.71
over (min)	2.50	2.50
Storage Coeff. (min)=	1.41 (ii)	3.38 (ii)
Unit Hyd. Tpeak (min)=	2.50	2.50
Unit Hyd. peak (cms)=	.56	.36

			TOTALS
PEAK FLOW	(cms)=	.17	.16
TIME TO PEAK	(hrs)=	1.25	1.25
RUNOFF VOLUME	(mm)=	42.47	30.51
TOTAL RAINFALL	(mm)=	44.47	44.47
RUNOFF COEFFICIENT	=	.96	.69
			.335 (iii)
			1.250
			35.292
			44.466
			.794

*** WARNING: Storage Coefficient is smaller than DT!
 Use a smaller DT or a larger area.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 95.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 005:0004-----

*=====

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* TRIBUTARY AREAS TO ADJACENT PROPERTY TO THE WEST (UNCONTROLLED)

*=====

| CALIB STANDHYD | Area (ha)= 1.13
| 07:302 DT= 2.00 | Total Imp(%)= 45.00 Dir. Conn.(%)= 40.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	.51	.62
Dep. Storage	(mm)=	2.00	5.00
Average Slope	(%)=	1.80	2.00
Length	(m)=	105.00	5.50
Mannings n	=	.015	.250

*** NOTE: User defined Storage Coefficients were used
for Unit Hydrograph calculations.

Max.eff.Inten.(mm/hr)=	141.20	112.76
over (min)	2.50	5.00
Storage Coeff. (min)=	2.00 (ii)	4.05 (ii)
Unit Hyd. Tpeak (min)=	2.50	5.00
Unit Hyd. peak (cms)=	.48	.25

			TOTALS
PEAK FLOW	(cms)=	.17	.14
TIME TO PEAK	(hrs)=	1.25	1.29
RUNOFF VOLUME	(mm)=	42.47	30.51
TOTAL RAINFALL	(mm)=	44.47	44.47
RUNOFF COEFFICIENT	=	.96	.69

*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 95.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

005:0005-----

ADD HYD (	303)	ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF
(cms)							
		ID1 06:301	1.13	.335	1.25	35.29	
.000							
		+ID2 07:302	1.13	.285	1.25	35.29	
.000							

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SUM 08:	303	2.26	.620	1.25	35.29
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.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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005:0006-----
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005:0002-----
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005:0002-----
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** END OF RUN : 9

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| START          | Project dir.: Q:\55926\100\202505~1\SWMHYMO\
----- Rainfall dir.: Q:\55926\100\202505~1\SWMHYMO\
```

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TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 010
NSTORM= 1
# 1=10YR.HYT
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010:0002-----
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*#*****
**

*# Project Name: [GLENDON ROAD] Project Number: [55926-100]

*# Date : OCTOBER 2024

*# Modeller : [JJM]

*# Company : MTE CONSULTANTS INC.

*# License # :

*#*****
**

010:0002

READ STORM
Ptotal= 52.37 mm

Filename: 10YR Chicago 3-hr duration
Comments: 10YR Chicago 3-hr duration

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	3.141	.92	11.986	1.75	13.417	2.58	4.407
.17	3.389	1.00	16.365	1.83	11.203	2.67	4.128
.25	3.681	1.08	25.006	1.92	9.593	2.75	3.882
.33	4.030	1.17	47.536	2.00	8.375	2.83	3.665
.42	4.454	1.25	162.500	2.08	7.426	2.92	3.472
.50	4.979	1.33	92.425	2.17	6.667	3.00	3.298
.58	5.645	1.42	47.240	2.25	6.047	3.08	3.141
.67	6.517	1.50	30.137	2.33	5.531		
.75	7.701	1.58	21.600	2.42	5.097		
.83	9.394	1.67	16.623	2.50	4.727		

010:0003

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* TRIBUTARY AREAS TO STREET A SOUTH TO GLENDON DRIVE (UNCONTROLLED)

*=====

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CALIB STANDHYD
06:301 DT= 2.00

Area (ha)= 1.13
Total Imp(%)= 45.00 Dir. Conn.(%)= 40.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)=	.51	.62	
Dep. Storage (mm)=	2.00	5.00	
Average Slope (%)=	2.00	2.00	
Length (m)=	57.00	5.50	
Mannings n =	.015	.250	
Max.eff.Inten.(mm/hr)=	162.50	148.58	
over (min)	2.50	2.50	
Storage Coeff. (min)=	1.33 (ii)	3.16 (ii)	
Unit Hyd. Tpeak (min)=	2.50	2.50	
Unit Hyd. peak (cms)=	.58	.37	
			TOTALS
PEAK FLOW (cms)=	.20	.20	.405 (iii)
TIME TO PEAK (hrs)=	1.25	1.25	1.250
RUNOFF VOLUME (mm)=	50.37	38.03	42.967
TOTAL RAINFALL (mm)=	52.37	52.37	52.369
RUNOFF COEFFICIENT =	.96	.73	.820

*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 95.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

010:0004

*=====

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* TRIBUTARY AREAS TO ADJACENT PROPERTY TO THE WEST (UNCONTROLLED)

*=====

=

CALIB STANDHYD	Area (ha)=	1.13
07:302 DT= 2.00	Total Imp(%)=	45.00 Dir. Conn.(%)= 40.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	.51	.62
Dep. Storage	(mm)=	2.00	5.00
Average Slope	(%)=	1.80	2.00
Length	(m)=	105.00	5.50
Mannings n	=	.015	.250

*** NOTE: User defined Storage Coefficients were used
for Unit Hydrograph calculations.

Max.eff.Inten.(mm/hr)=	162.50	139.10
over (min)	2.50	5.00
Storage Coeff. (min)=	2.00 (ii)	3.88 (ii)
Unit Hyd. Tpeak (min)=	2.50	5.00
Unit Hyd. peak (cms)=	.48	.26

			TOTALS
PEAK FLOW (cms)=	.19	.18	.345 (iii)
TIME TO PEAK (hrs)=	1.25	1.29	1.250
RUNOFF VOLUME (mm)=	50.37	38.03	42.967
TOTAL RAINFALL (mm)=	52.37	52.37	52.369
RUNOFF COEFFICIENT =	.96	.73	.820

*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 95.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0002-----

*#*****
**
*# Project Name: [GLENDON ROAD] Project Number: [55926-100]

*# Date : OCTOBER 2024

*# Modeller : [JJM]

*# Company : MTE CONSULTANTS INC.

*# License # :

*#*****
**

025:0002-----

READ STORM		Filename: 25YR Chicago 3-hr duration
Ptotal= 61.85 mm		Comments: 25YR Chicago 3-hr duration

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	3.490	.92	14.107	1.75	15.861	2.58	4.972
.17	3.779	1.00	19.457	1.83	13.158	2.67	4.644
.25	4.120	1.08	30.035	1.92	11.200	2.75	4.356
.33	4.529	1.17	57.437	2.00	9.725	2.83	4.101
.42	5.028	1.25	190.801	2.08	8.578	2.92	3.875
.50	5.649	1.33	111.064	2.17	7.665	3.00	3.672
.58	6.442	1.42	57.174	2.25	6.922	3.08	3.490
.67	7.484	1.50	36.348	2.33	6.307		
.75	8.908	1.58	25.889	2.42	5.790		
.83	10.956	1.67	19.786	2.50	5.351		

025:0003-----

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* TRIBUTARY AREAS TO STREET A SOUTH TO GLENDON DRIVE (UNCONTROLLED)

*=====

=

CALIB STANDHYD		Area (ha)=	1.13		
06:301 DT= 2.00		Total Imp(%)=	45.00	Dir. Conn.(%)=	40.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	.51	.62
Dep. Storage	(mm)=	2.00	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	57.00	5.50
Mannings n	=	.015	.250

Max.eff.Inten.(mm/hr)=		190.80	181.86
over (min)		2.50	2.50
Storage Coeff. (min)=	1.25 (ii)		2.94 (ii)
Unit Hyd. Tpeak (min)=		2.50	2.50
Unit Hyd. peak (cms)=		.59	.39

TOTALS

PEAK FLOW	(cms)=	.24	.26	.497 (iii)
TIME TO PEAK	(hrs)=	1.25	1.25	1.250
RUNOFF VOLUME	(mm)=	59.85	47.17	52.239
TOTAL RAINFALL	(mm)=	61.85	61.85	61.846
RUNOFF COEFFICIENT	=	.97	.76	.845

*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 95.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

025:0004-

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* TRIBUTARY AREAS TO ADJACENT PROPERTY TO THE WEST (UNCONTROLLED)

*=====

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CALIB STANDHYD	Area	(ha)=	1.13	
07:302 DT= 2.00	Total Imp(%)=	45.00	Dir. Conn.(%)=	40.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	.51	.62
Dep. Storage	(mm)=	2.00	5.00
Average Slope	(%)=	1.80	2.00
Length	(m)=	105.00	5.50
Mannings n	=	.015	.250

*** NOTE: User defined Storage Coefficients were used
for Unit Hydrograph calculations.

Max.eff.Inten.(mm/hr)=		190.80	181.86
over (min)		2.50	2.50
Storage Coeff. (min)=	2.00 (ii)		3.69 (ii)

Unit Hyd. Tpeak (min)=	2.50	2.50	
Unit Hyd. peak (cms)=	.48	.33	
			TOTALS
PEAK FLOW (cms)=	.23	.24	.466 (iii)
TIME TO PEAK (hrs)=	1.25	1.25	1.250
RUNOFF VOLUME (mm)=	59.85	47.17	52.239
TOTAL RAINFALL (mm)=	61.85	61.85	61.846
RUNOFF COEFFICIENT =	.97	.76	.845

*** WARNING: Storage Coefficient is smaller than DT!
 Use a smaller DT or a larger area.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 95.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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025:0005-----
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-----
| ADD HYD (      303) | ID: NHYD      AREA      QPEAK      TPEAK      R.V.      DWF
-----
(cms)
                ID1 06:301          1.13      .497      1.25      52.24
.000
                +ID2 07:302          1.13      .466      1.25      52.24
.000

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                SUM 08:      303      2.26      .962      1.25      52.24
.000
  
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NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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025:0006-----
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025:0002-----
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025:0002-----
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025:0002-----
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025:0002-----

** END OF RUN : 49

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| START | Project dir.: Q:\55926\100\202505~1\SWMHYMO\

----- Rainfall dir.: Q:\55926\100\202505~1\SWMHYMO\

TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 050
NSTORM= 1
1=50YR.HYT

050:0002-----

*#*****
**

*# Project Name: [GLENDON ROAD] Project Number: [55926-100]

*# Date : OCTOBER 2024

*# Modeller : [JJM]

*# Company : MTE CONSULTANTS INC.

*# License # :

*#*****
**

050:0002-----

| READ STORM | Filename: 50YR Chicago 3-hr duration
| Ptotal= 69.13 mm | Comments: 50YR Chicago 3-hr duration

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	3.895	.92	15.824	1.75	17.797	2.58	5.558
.17	4.219	1.00	21.837	1.83	14.758	2.67	5.189
.25	4.601	1.08	33.713	1.92	12.556	2.75	4.866

.33	5.060		1.17	64.387		2.00	10.897		2.83	4.580
.42	5.620		1.25	212.001		2.08	9.609		2.92	4.326
.50	6.318		1.33	124.085		2.17	8.582		3.00	4.100
.58	7.208		1.42	64.104		2.25	7.747		3.08	3.895
.67	8.379		1.50	40.797		2.33	7.057			
.75	9.980		1.58	29.062		2.42	6.476			
.83	12.281		1.67	22.208		2.50	5.983			

 050:0003-----

*=====

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* TRIBUTARY AREAS TO STREET A SOUTH TO GLENDON DRIVE (UNCONTROLLED)

*=====

=

CALIB STANDHYD		Area	(ha)=	1.13			
06:301 DT= 2.00		Total Imp(%)=	45.00	Dir. Conn.(%)=	40.00		

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	.51	.62
Dep. Storage	(mm)=	2.00	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	57.00	5.50
Mannings n	=	.015	.250

Max.eff.Inten.(mm/hr)=	212.00	206.72
over (min)	2.50	2.50
Storage Coeff. (min)=	1.19 (ii)	2.80 (ii)
Unit Hyd. Tpeak (min)=	2.50	2.50
Unit Hyd. peak (cms)=	.60	.40

			TOTALS
PEAK FLOW	(cms)=	.26	.30
TIME TO PEAK	(hrs)=	1.25	1.25
RUNOFF VOLUME	(mm)=	67.13	54.25
TOTAL RAINFALL	(mm)=	69.13	69.13
RUNOFF COEFFICIENT	=	.97	.78
			.566 (iii)
			1.250
			59.400
			69.130
			.859

*** WARNING: Storage Coefficient is smaller than DT!
 Use a smaller DT or a larger area.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 95.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

 050:0004-----

*=====

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* TRIBUTARY AREAS TO ADJACENT PROPERTY TO THE WEST (UNCONTROLLED)

*=====

=

CALIB STANDHYD		Area (ha)=	1.13		
07:302 DT= 2.00		Total Imp(%)=	45.00	Dir. Conn.(%)=	40.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	.51	.62
Dep. Storage	(mm)=	2.00	5.00
Average Slope	(%)=	1.80	2.00
Length	(m)=	105.00	5.50
Mannings n	=	.015	.250

*** NOTE: User defined Storage Coefficients were used
for Unit Hydrograph calculations.

Max.eff.Inten.(mm/hr)=	212.00	206.72
over (min)	2.50	2.50
Storage Coeff. (min)=	2.00 (ii)	3.61 (ii)
Unit Hyd. Tpeak (min)=	2.50	2.50
Unit Hyd. peak (cms)=	.48	.34

			TOTALS
PEAK FLOW	(cms)=	.25	.28
TIME TO PEAK	(hrs)=	1.25	1.25
RUNOFF VOLUME	(mm)=	67.13	54.25
TOTAL RAINFALL	(mm)=	69.13	69.13
RUNOFF COEFFICIENT	=	.97	.78
			.528 (iii)
			1.250
			59.400
			69.130
			.859

*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 95.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

050:0005-----

ADD HYD (303)	ID: NHYD	AREA	QPEAK	TPEAK	R.V.	DWF
-----		(ha)	(cms)	(hrs)	(mm)	
(cms)						
	ID1 06:301	1.13	.566	1.25	59.40	
.000						
	+ID2 07:302	1.13	.528	1.25	59.40	
.000						

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.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

050:0006.

050:0002.

050:0002.

050:0002.

050:0002.

050:0002.

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** END OF RUN : 99
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| START

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Project dir.: Q:\55926\100\202505~1\SWMHYMO\
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----- Rainfall dir.: Q:\55926\100\202505~1\SWMHYMO\
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TZERO = .00 hrs on 0

METOUT= 2 (output = METRIC)

NRUN = 100

NSTORM= 1

1=100YR.HYT

100:0002.

*#*****

**

*# Project Name: [GLENDON ROAD] Project Number: [55926-100]

*# Date : OCTOBER 2024

*# Modeller : [JJM]

*# Company : MTE CONSULTANTS INC.

*# License # :

**

100:0002

| READ STORM | Filename: 100YR Chicago 3-hr duration
| Ptotal= 76.27 mm | Comments: 100YR Chicago 3-hr duration

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.08	4.164	.92	17.483	1.75	19.709	2.58	5.997
.17	4.519	1.00	24.251	1.83	16.288	2.67	5.589
.25	4.940	1.08	37.617	1.92	13.813	2.75	5.232
.33	5.447	1.17	71.935	2.00	11.952	2.83	4.917
.42	6.066	1.25	232.200	2.08	10.509	2.92	4.638
.50	6.839	1.33	137.906	2.17	9.361	3.00	4.388
.58	7.828	1.42	71.694	2.25	8.430	3.08	4.164
.67	9.133	1.50	45.604	2.33	7.661		
.75	10.922	1.58	32.403	2.42	7.015		
.83	13.502	1.67	24.679	2.50	6.467		

100:0003

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* TRIBUTARY AREAS TO STREET A SOUTH TO GLENDON DRIVE (UNCONTROLLED)

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| CALIB STANDHYD | Area (ha)= 1.13
| 06:301 DT= 2.00 | Total Imp(%)= 45.00 Dir. Conn.(%)= 40.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	.51	.62
Dep. Storage	(mm)=	2.00	5.00
Average Slope	(%)=	2.00	2.00
Length	(m)=	57.00	5.50

Mannings n	=	.015	.250	
Max.eff.Inten.(mm/hr)=		232.20	230.25	
over (min)		2.50	2.50	
Storage Coeff. (min)=		1.15 (ii)	2.69 (ii)	
Unit Hyd. Tpeak (min)=		2.50	2.50	
Unit Hyd. peak (cms)=		.60	.41	
				TOTALS
PEAK FLOW (cms)=		.29	.34	.632 (iii)
TIME TO PEAK (hrs)=		1.25	1.25	1.250
RUNOFF VOLUME (mm)=		74.27	61.22	66.443
TOTAL RAINFALL (mm)=		76.27	76.27	76.272
RUNOFF COEFFICIENT =		.97	.80	.871

*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 95.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0004-----

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* TRIBUTARY AREAS TO ADJACENT PROPERTY TO THE WEST (UNCONTROLLED)
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| CALIB STANDHYD | Area (ha)= 1.13
| 07:302 DT= 2.00 | Total Imp(%)= 45.00 Dir. Conn.(%)= 40.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	.51	.62
Dep. Storage	(mm)=	2.00	5.00
Average Slope	(%)=	1.80	2.00
Length	(m)=	105.00	5.50
Mannings n	=	.015	.250

*** NOTE: User defined Storage Coefficients were used
for Unit Hydrograph calculations.

Max.eff.Inten.(mm/hr)=		232.20	230.25	
over (min)		2.50	2.50	
Storage Coeff. (min)=		2.00 (ii)	3.54 (ii)	
Unit Hyd. Tpeak (min)=		2.50	2.50	
Unit Hyd. peak (cms)=		.48	.34	
				TOTALS
PEAK FLOW (cms)=		.27	.31	.589 (iii)
TIME TO PEAK (hrs)=		1.25	1.25	1.250

RUNOFF VOLUME	(mm)=	74.27	61.22	66.443
TOTAL RAINFALL	(mm)=	76.27	76.27	76.272
RUNOFF COEFFICIENT	=	.97	.80	.871

*** WARNING: Storage Coefficient is smaller than DT!
 Use a smaller DT or a larger area.

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
 CN* = 95.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
 THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

100:0005-----							

ADD HYD (	303)	ID: NHYD	AREA	QPEAK	TPEAK	R.V.	DWF
-----			(ha)	(cms)	(hrs)	(mm)	
(cms)							
		ID1 06:301	1.13	.632	1.25	66.44	
.000							
		+ID2 07:302	1.13	.589	1.25	66.44	
.000							
=====							
		SUM 08:	303	2.26	1.220	1.25	66.44
.000							

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

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100:0006-----
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100:0002-----
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100:0002-----
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100:0002-----
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FINISH
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WARNINGS / ERRORS / NOTES
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001:0003 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
            Use a smaller DT or a larger area.
001:0004 CALIB STANDHYD
*** NOTE: User defined Storage Coefficients were used
            for Unit Hydrograph calculations.
*** WARNING: Storage Coefficient is smaller than DT!
            Use a smaller DT or a larger area.
002:0003 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
            Use a smaller DT or a larger area.
002:0004 CALIB STANDHYD
*** NOTE: User defined Storage Coefficients were used
            for Unit Hydrograph calculations.
*** WARNING: Storage Coefficient is smaller than DT!
            Use a smaller DT or a larger area.
005:0003 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
            Use a smaller DT or a larger area.
005:0004 CALIB STANDHYD
*** NOTE: User defined Storage Coefficients were used
            for Unit Hydrograph calculations.
*** WARNING: Storage Coefficient is smaller than DT!
            Use a smaller DT or a larger area.
010:0003 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
            Use a smaller DT or a larger area.
010:0004 CALIB STANDHYD
*** NOTE: User defined Storage Coefficients were used
            for Unit Hydrograph calculations.
*** WARNING: Storage Coefficient is smaller than DT!
            Use a smaller DT or a larger area.
025:0003 CALIB STANDHYD
*** WARNING: Storage Coefficient is smaller than DT!
            Use a smaller DT or a larger area.
025:0004 CALIB STANDHYD
*** NOTE: User defined Storage Coefficients were used
            for Unit Hydrograph calculations.
*** WARNING: Storage Coefficient is smaller than DT!
            Use a smaller DT or a larger area.

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050:0003 CALIB STANDHYD

*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

050:0004 CALIB STANDHYD

*** NOTE: User defined Storage Coefficients were used
for Unit Hydrograph calculations.

*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

100:0003 CALIB STANDHYD

*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

100:0004 CALIB STANDHYD

*** NOTE: User defined Storage Coefficients were used
for Unit Hydrograph calculations.

*** WARNING: Storage Coefficient is smaller than DT!
Use a smaller DT or a larger area.

Simulation ended on 2025-05-27 at 13:53:49

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